

Gas Accretion onto a Supermassive Black Hole: a step to modeling AGN feedback in cosmological simulations

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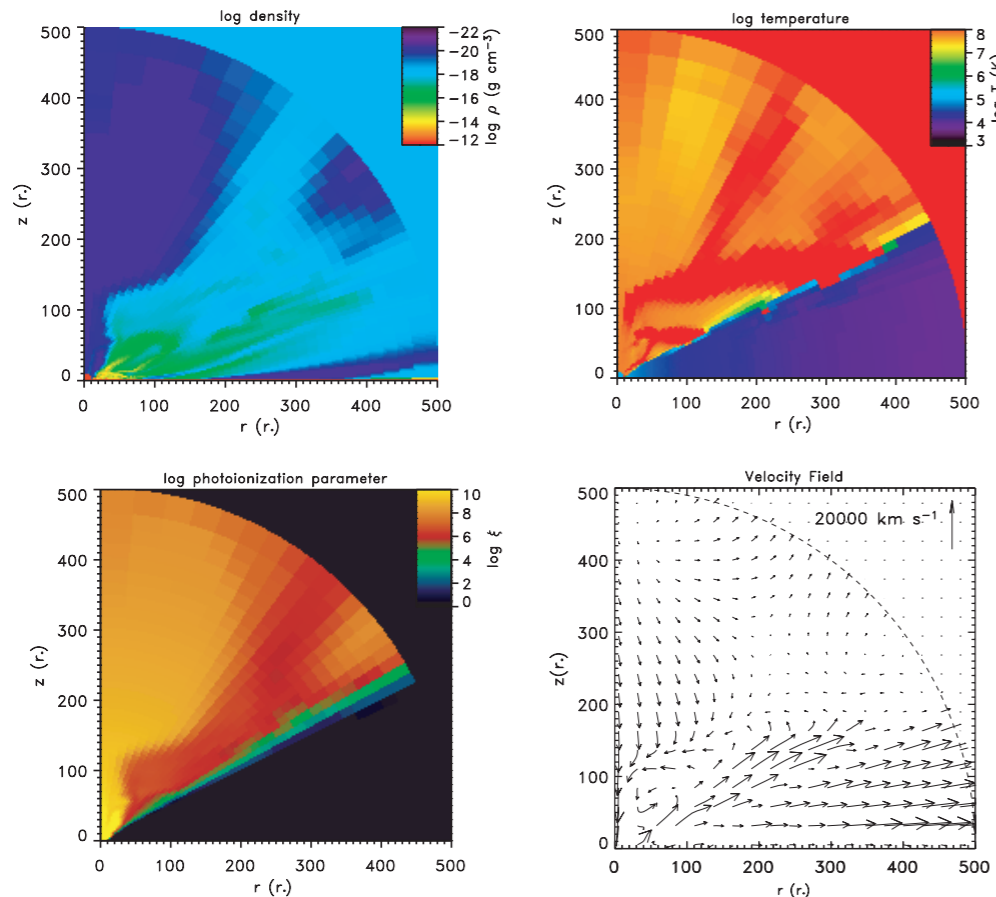
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Daniel Proga (UNLV)

Outline

- Intro / Motivation
- The simplest case: spherical Bondi accretion
- Include radiative cooling / heating -- radiative feedback by X-rays Barai, Proga, KN, 2011, MNRAS, in press (arXiv:1102.3925)
- Non-spherical accretion flow, fragmentation due to thermal instability Barai, Proga, KN, 2011, in prep. (Paper II)
- Conclusions

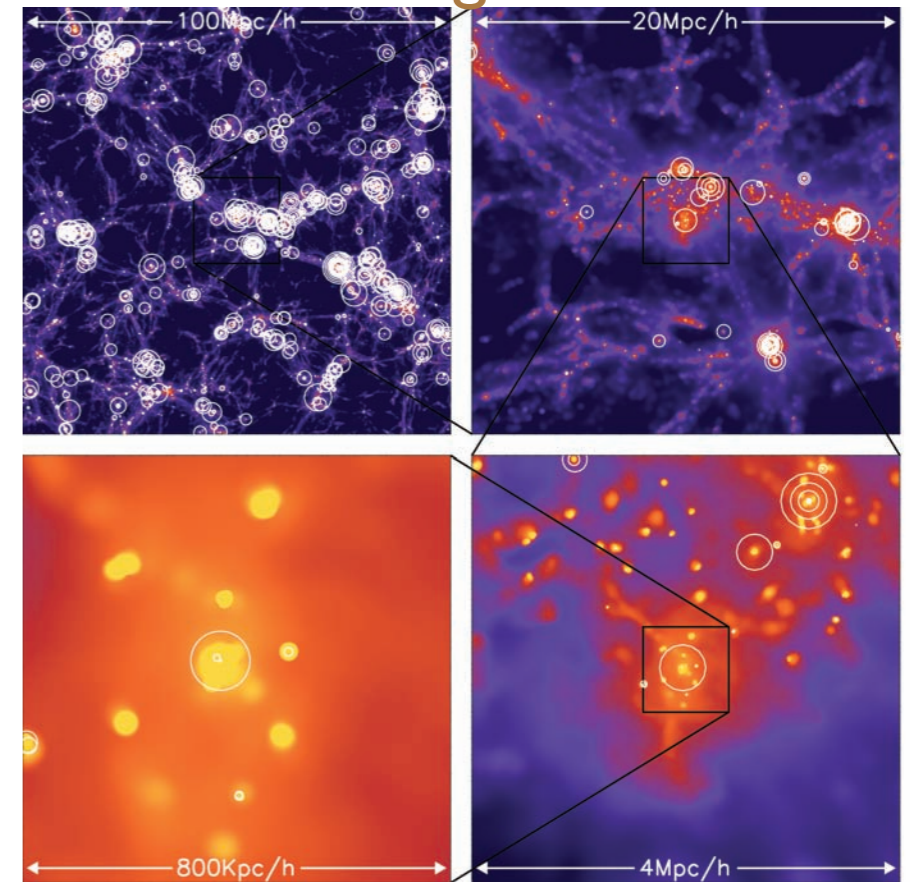
Motivation

Small-scale sims

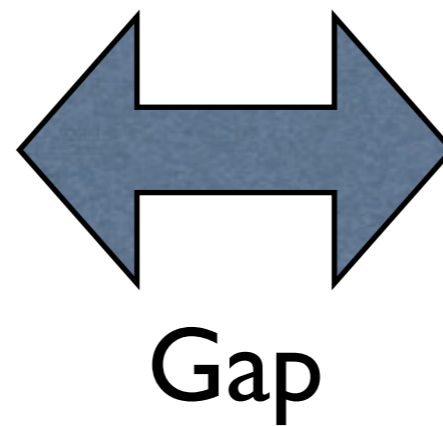


(e.g. Ohsuga, Proga, ...)

Cosmological sims



(e.g. Di Matteo+, Booth & Schaye, ...)



- Still a large gap btw **small-scale** sims & **cosmological** sims.
($\approx \text{pc}$) ($\sim \text{kpc} - 10 \text{ Mpc}$)
- Cosmo sims uses ad-hoc AGN accretion models as “sub-grid” physics.
- How well can a cosmological SPH code (e.g. GADGET) handle accretion onto a SMBH?

The Bondi Accretion Problem

- Spherically symmetric accretion onto a central mass (Bondi 1952)
- Gas is at rest at infinity, with ρ_∞ & p_∞ . Increase in the central mass is ignored.
- Two equations are solved:

$$\dot{M} = -4\pi r^2 \rho v = \text{constant.} \quad (\text{Continuity Eq.})$$

$$\frac{v^2}{2} + \left(\frac{\gamma}{\gamma - 1} \right) \frac{p_\infty}{\rho_\infty} \left[\left(\frac{\rho}{\rho_\infty} \right)^{\gamma-1} - 1 \right] = \frac{GM_{BH}}{r}, \quad (\text{Bernoulli's Eq.})$$

- One of the solutions:

$$\dot{M}_B = 4\pi \lambda_c \frac{(GM_{BH})^2}{c_{s,\infty}^3} \rho_\infty, \quad \lambda_c = \left(\frac{1}{2} \right)^{\frac{(\gamma+1)}{2(\gamma-1)}} \left(\frac{5-3\gamma}{4} \right)^{\frac{(3\gamma-5)}{2(\gamma-1)}}.$$

- Characteristic scales:

$$\text{Bondi radius: } R_B = \frac{GM_{BH}}{c_{s,\infty}^2}. \quad \text{Sonic radius: } R_s = \left(\frac{5-3\gamma}{4} \right) R_B.$$

$$\text{Bondi time: } t_B = \frac{R_B}{c_s} = \frac{GM_{BH}}{c_{s,\infty}^3}.$$

Simplest Case: Spherical Bondi Accretion Flow onto a SMBH

- GADGET-3: 3-d cosmological SPH/N-body code (Springel '05)
- **Central SMBH $10^8 M_\odot$**
represented by a pseudo-Newtonian Paczynsky & Wiita (1980) potential
- $r_{\text{out}}=5-20 \text{ pc}$, $N_{\text{ptcl}}=64^3-128^3$
- Set IC to uniform/spherical Bondi flow w/ $\gamma=1.01$, $\rho_\infty=10^{-19} \text{ g/cm}^3$, $T_\infty=10^7 \text{ K}$, $T_{\text{init}}=T_\infty$
- Corresponding Bondi solution: $R_B=3 \text{ pc}$, $R_{\text{sonic}}=1.5 \text{ pc}$, $t_B=7.9 \text{ e3yr}$
- All runs: $r_{\text{in}}=0.1 \text{ pc}$, $\gamma=1.01$

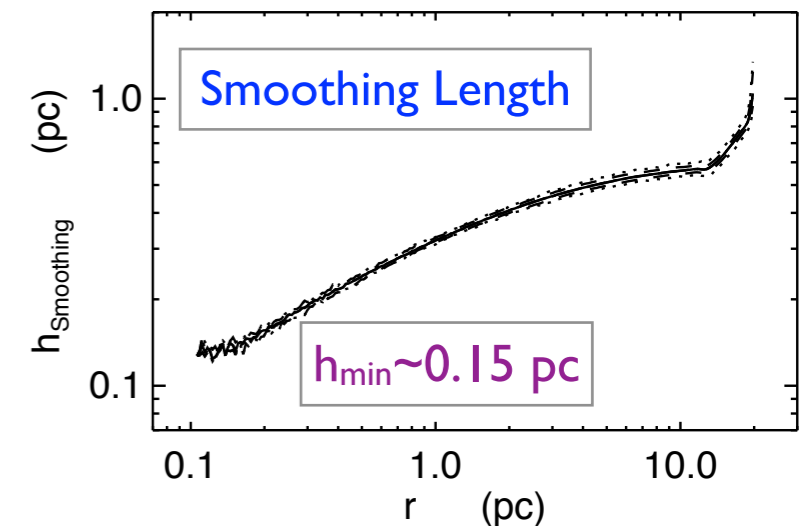
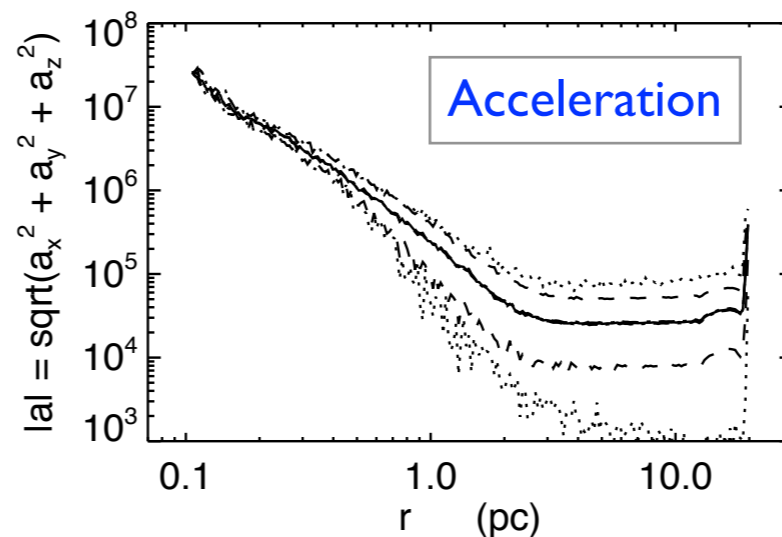
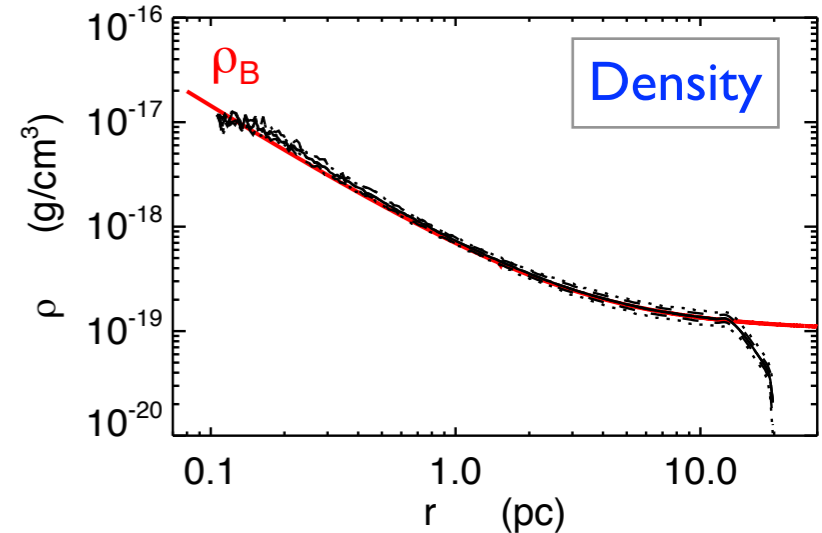
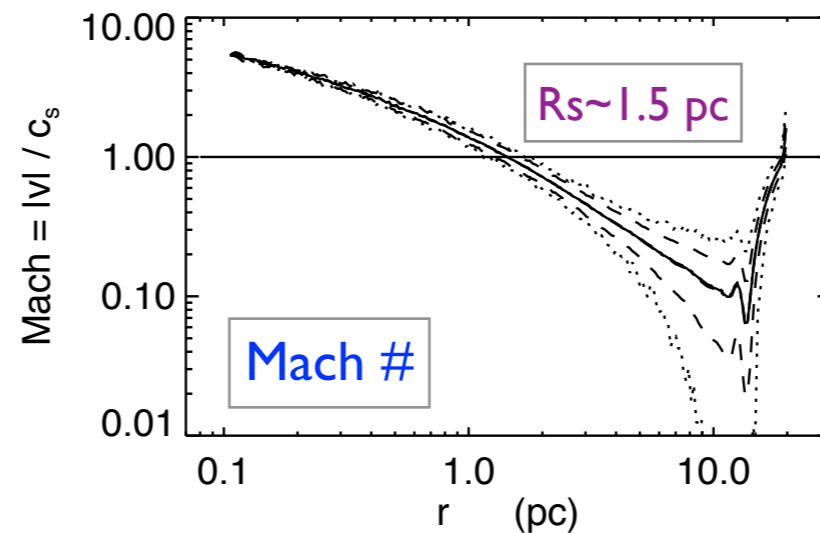
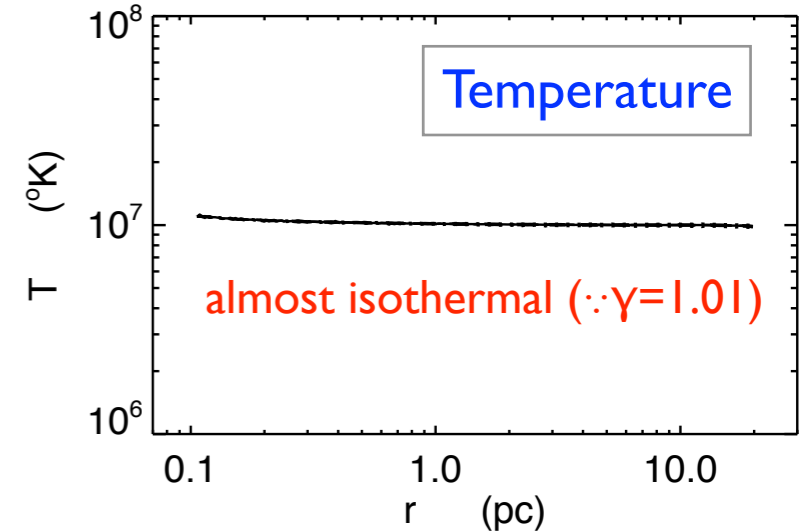
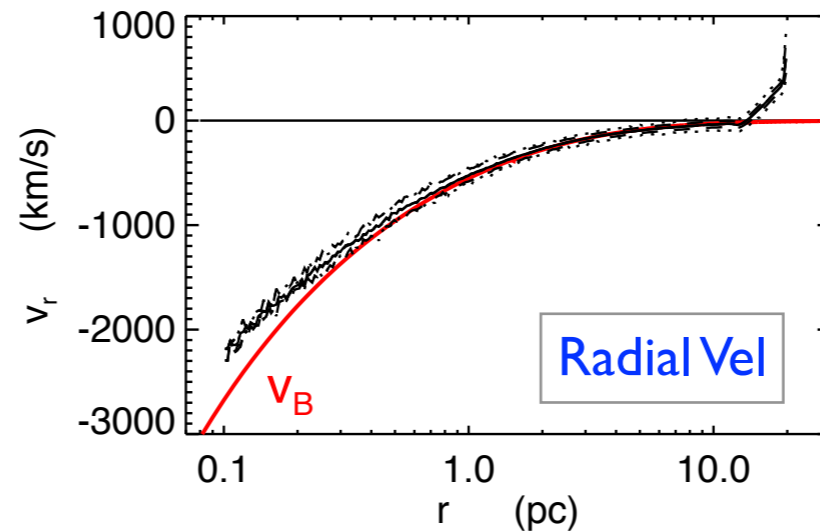
3-d spherical volume, vacuum boundary condition

Run No.	r_{out} [pc]	N^b	IC	$M_{\text{tot,IC}}^c$ [M_\odot]	M_{part}^d [M_\odot]	t_{end}^e [10^4 yr]
1	5	64^3	Uniform ⁱ	3.96×10^5	1.51	3
2	10	64^3	Uniform	6.19×10^6	23.61	7.2
3	50	128^3	Uniform	7.73×10^8	368.60	20
4	5	64^3	Bondi ^j	1.81×10^6	6.89	2
5	10	64^3	Bondi	9.76×10^6	37.23	8
6	10	128^3	Bondi	9.76×10^6	4.65	8
7	20	128^3	Bondi	6.24×10^7	29.75	8
7a ^k	20	128^3	Bondi	6.24×10^7	29.75	80
7b ^l	20	128^3	Bondi	6.24×10^7	29.75	100
8	50	128^3	Bondi	8.48×10^8	404.35	16
9	20	128^3	$\rho_B, v_{\text{init}} = 0$	6.24×10^7	29.75	8
10	20	128^3	Uniform	4.95×10^7	23.60	8
11	20	128^3	Hernquist ^m	6.24×10^7	29.75	7.2
12 ⁿ	20	128^3	Bondi	6.24×10^7	29.75	8

Example: Properties of Particles

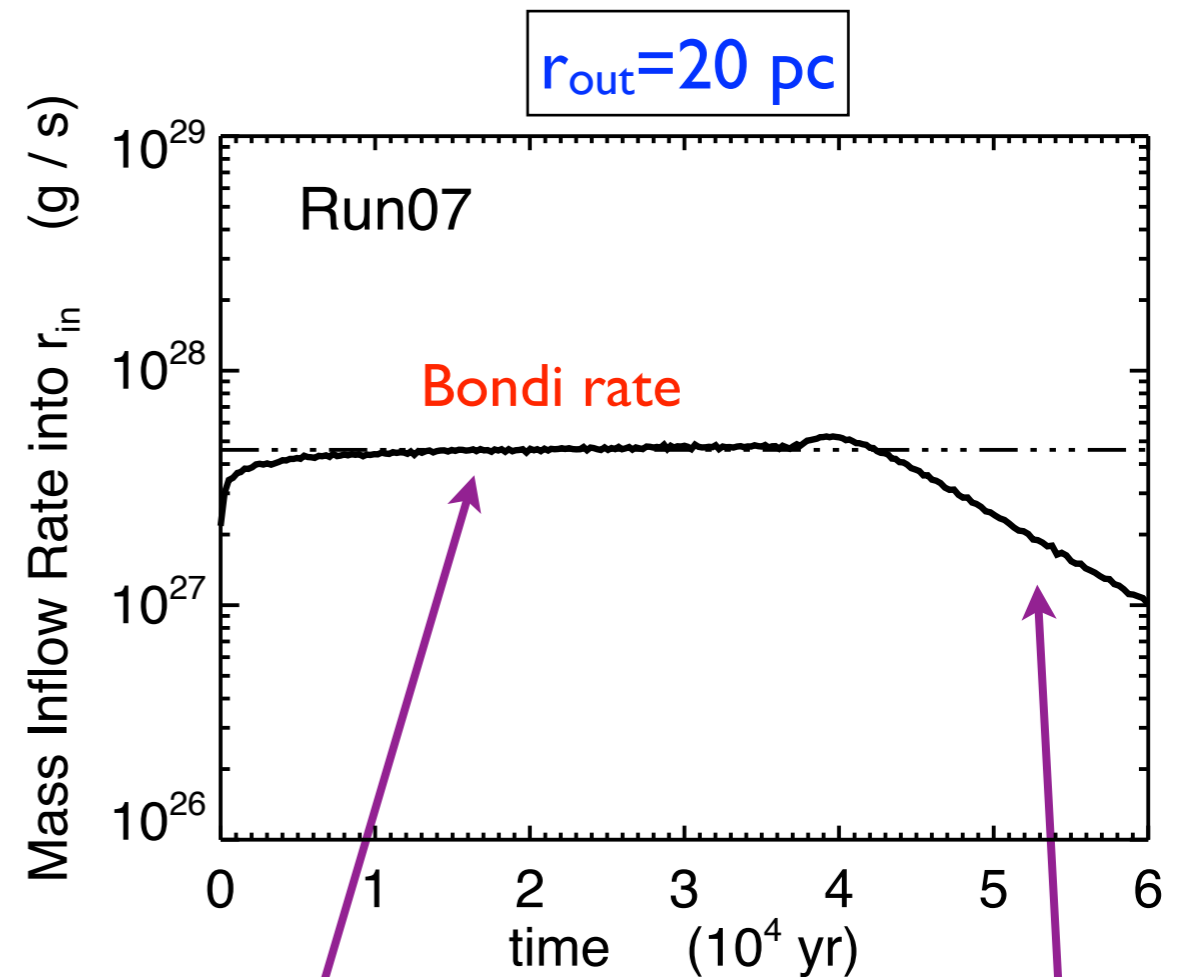
Run 7:

- $r_{\text{out}}=20 \text{ pc}$, $N_{\text{ptcl}}=128^3$
- Snap at $t=2t_B=1.6e4 \text{ yr}$
- Follows the **Bondi solution (red curve)** well except the very inner part
- Inner part: supersonic ($M\sim 6$), outerpart: subsonic



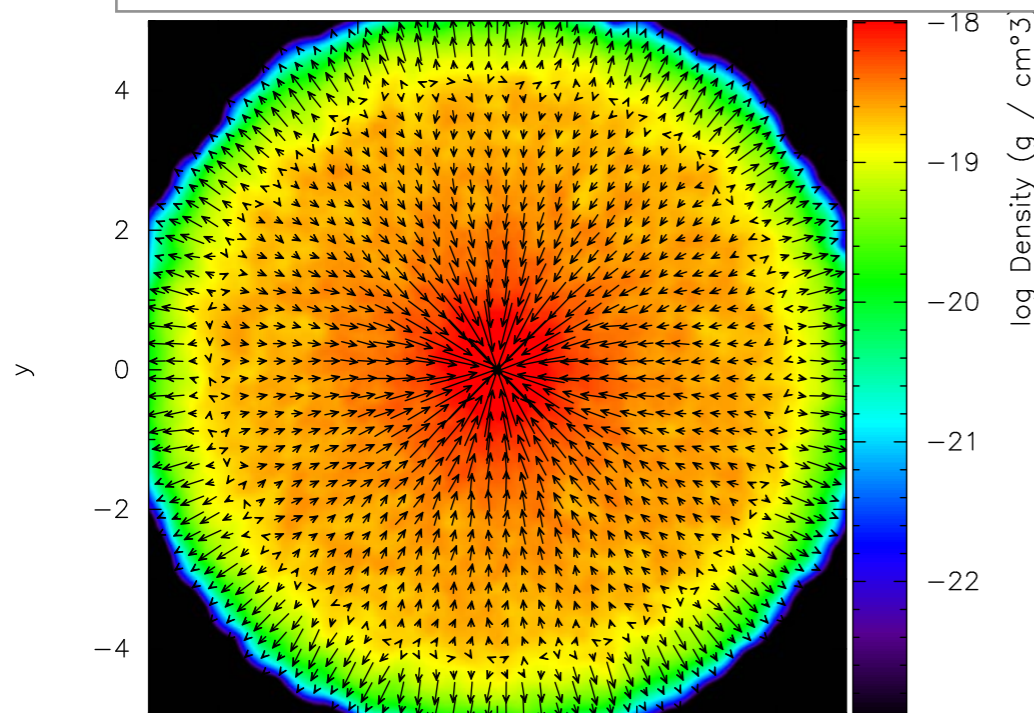
Mass Inflow Rates at r_{in}

- the larger r_{out} , the longer duration of Bondi inflow rate
- If started from a Bondi flow, Bondi rate is achieved quickly.
- After a while, the inflow rate decreases due to the artificial outflow at the outer boundary.
- Greater sim. volume reduces this effect on mass inflow.



reproducing Bondi rate well.

due to outflow problem at outer BC



Radiative Heating & Cooling

- Xray emitting corona irradiates the accretion flow

$$L_X = f_X L_{\text{Edd}}, \quad L_{\text{Edd}} = \frac{4\pi c G m_p M_{\text{BH}}}{\sigma_e}, \quad \text{Flux: } F_X = \frac{L_X}{4\pi r^2}.$$

- Approx. analytic heating/cooling rates from Blondin '94; opt-thin gas illuminated by a 10 keV bremsstrahlung.

net rate: $\rho \mathcal{L} = n^2 (G_{\text{Compton}} + G_X - L_{b,l}) \quad [\text{erg cm}^{-3} \text{ s}^{-1}],$

Compton h/c rate: $G_{\text{Compton}} = 8.9 \times 10^{-36} \xi (T_X - 4T) \quad [\text{erg cm}^3 \text{ s}^{-1}].$

Net Xray photoioniz. heating and recomb. cooling rate: $G_X = 1.5 \times 10^{-21} \xi^{1/4} T^{-1/2} \left(1 - \frac{T}{T_X}\right) \quad [\text{erg cm}^3 \text{ s}^{-1}].$

Brems. and line cooling rate:
(Opt-thin: $\delta=1$) $L_{b,l} = 3.3 \times 10^{-27} T^{1/2} + [1.7 \times 10^{-18} \exp(-1.3 \times 10^5/T) \xi^{-1} T^{-1/2} + 10^{-24}] \delta \quad [\text{erg cm}^3 \text{ s}^{-1}].$

$T_X = 1.16 \times 10^8 \text{ K} \quad (=10 \text{ keV, Blondin '94})$

Runs with radiative cooling/heating

Run No.	r_{out} [pc]	N	$M_{\text{tot,IC}} [M_{\odot}]$	$M_{\text{part}} [M_{\odot}]$	γ_{init}	T_{∞} [K]	R_B [pc]	ρ_{∞} [g/cm ³]	T_{init}	$L_X [L_{\text{Edd}}]$	$t_{\text{end}} [10^5 \text{ yr}]$
13	20	128 ³	5.81×10^5	0.277	1.4	10 ⁷	2.19	10 ⁻²¹	T_{∞}	0.5	1.0
14	50	128 ³	8.23×10^6	3.92	1.4	10 ⁷	2.19	10 ⁻²¹	T_{∞}	0.5	2.9
15	20	128 ³	5.81×10^{-1}	2.77×10^{-7}	1.4	10 ⁷	2.19	10 ⁻²⁷	T_{∞}	0.5	1.0
16	20	256 ³	5.81×10^{-1}	3.46×10^{-8}	1.4	10 ⁷	2.19	10 ⁻²⁷	T_{∞}	5×10^{-4}	1.9
17	20	128 ³	5.81×10^5	0.277	1.4	10 ⁷	2.19	10 ⁻²¹	T_{rad}^b	5×10^{-4}	2.9
18	20	128 ³	5.65×10^5	0.269	5/3	10 ⁷	1.84	10 ⁻²¹	T_{rad}	5×10^{-4}	3.0
19	20	128 ³	1.47×10^7	7.0	5/3	10 ⁵	183.9	10 ⁻²¹	T_{rad}	5×10^{-4}	1.5
20	200	256 ³	1.33×10^9	79.09	5/3	10 ⁵	183.9	10 ⁻²¹	T_{rad}	5×10^{-4}	6.5
21	200	256 ³	4.95×10^8	29.50	5/3	10 ⁷	1.84	10 ⁻²¹	T_{rad}	5×10^{-4}	8.7
22	200	128 ³	1.33×10^7	6.33	5/3	10 ⁵	183.9	10 ⁻²³	T_{rad}	5×10^{-4}	70
23	200	256 ³	1.33×10^7	0.791	5/3	10 ⁵	183.9	10 ⁻²³	T_{rad}	5×10^{-4}	20
24 ^c	200	1.24×10^7	9.77×10^6	0.791	5/3	10 ⁵	183.9	10 ⁻²³	T_{Run23}	5×10^{-5}	19
25	200	1.24×10^7	9.77×10^6	0.791	5/3	10 ⁵	183.9	10 ⁻²³	T_{Run23}	5×10^{-3}	21
26	200	1.24×10^7	9.77×10^6	0.791	5/3	10 ⁵	183.9	10 ⁻²³	T_{Run23}	1×10^{-2}	22
27	200	1.24×10^7	9.77×10^6	0.791	5/3	10 ⁵	183.9	10 ⁻²³	T_{Run23}	2×10^{-2}	25
28	200	1.24×10^7	9.77×10^6	0.791	5/3	10 ⁵	183.9	10 ⁻²³	T_{Run23}	5×10^{-2}	50

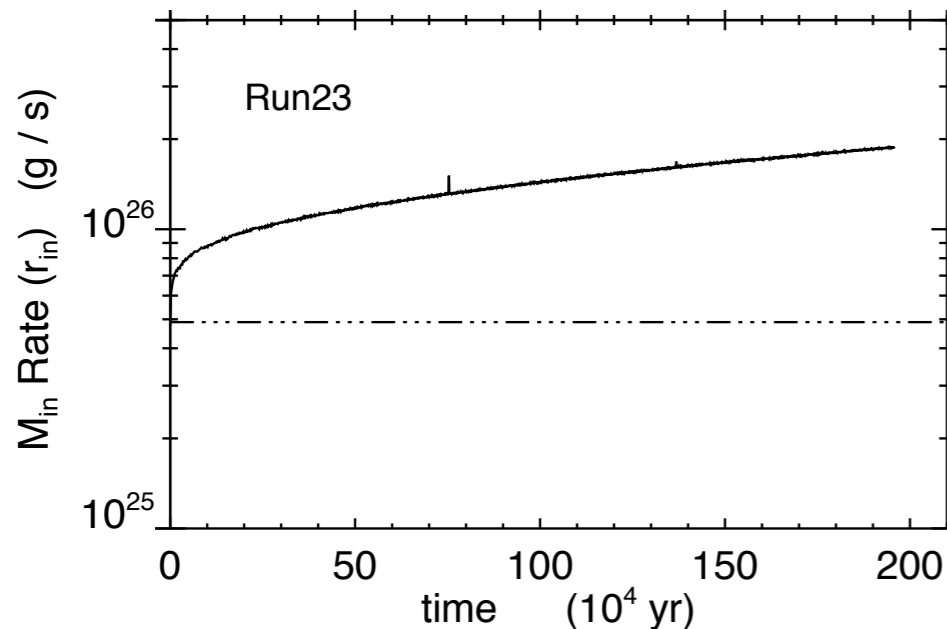
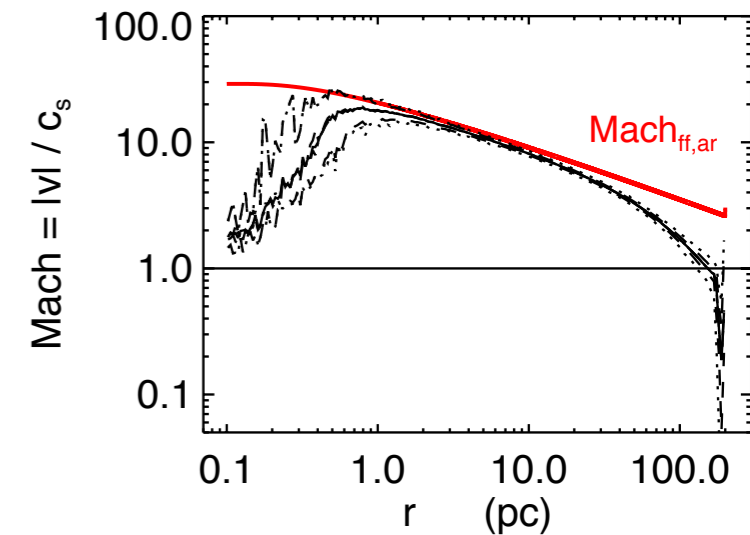
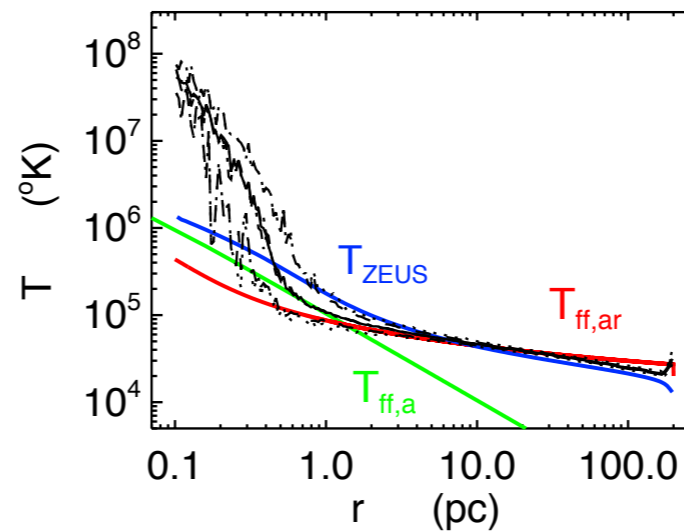
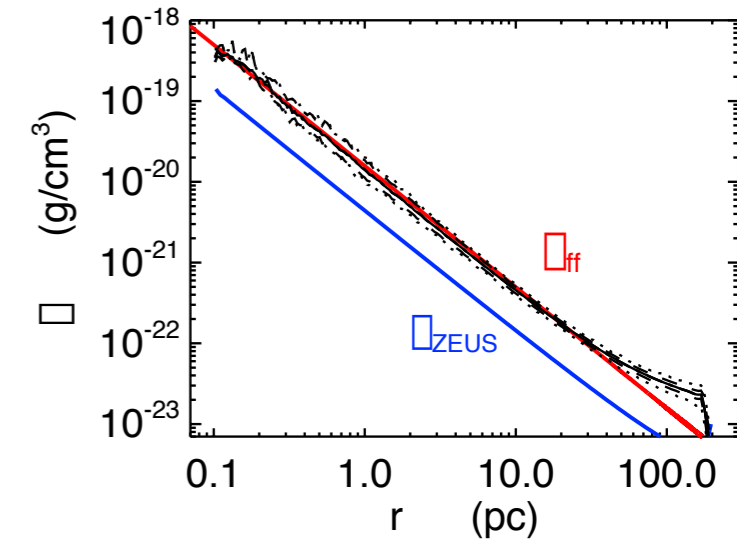
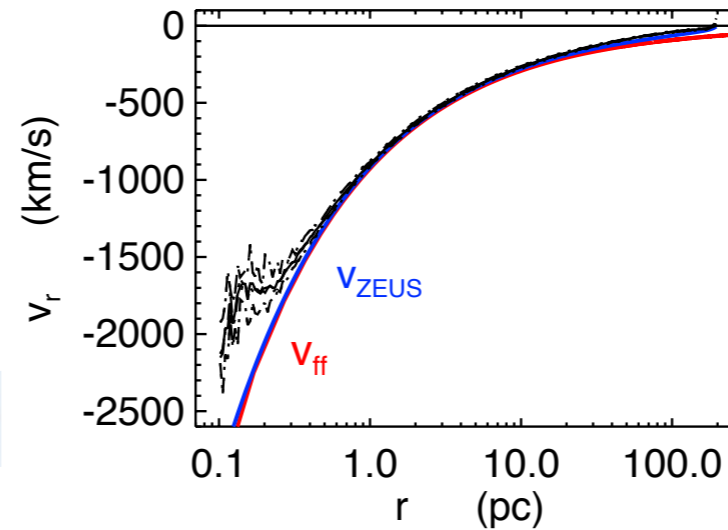
Ptcl properties w/ radiative heating & cooling

Representative run:

Run #23: $t=1\text{Myr}$, $L_X=5e-4L_{\text{Edd}}$, $\gamma=5/3$

$r_{\text{out}}=200\text{pc}$, 256^3 ptcls

- red: free-fall scaling
- blue: ZEUS-2d result
- Near the inner radius, excess heating by artificial viscosity is seen.
- Inflow rate is enhanced above Bondi rate, due to lower gas temp: $T(r_{\text{out}}) < 10^5 \text{ K}$, $T_\infty = 10^5 \text{ K}$

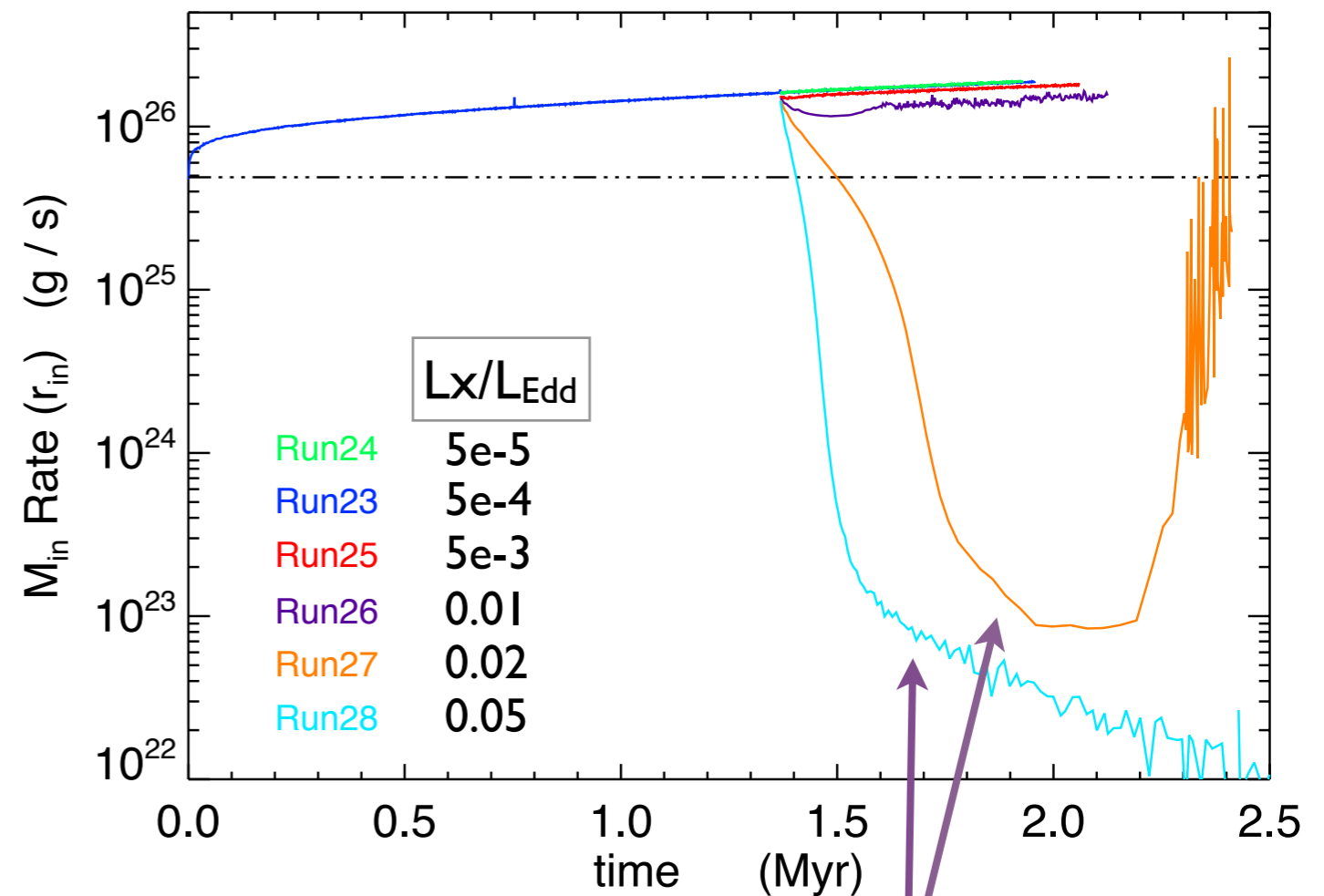


green: free-fall scaling w/ only adiabatic term

$T_{\text{ff,ar}}$: solving internal energy eq. w/ both radiative & adiabatic term

Impact of varying L_x on inflow rates

- Restart Run #23 at $t=1.4$ Myr, $L_x/L_{\text{Edd}}=5e-4$ orig.
- Runs 24-28: increase L_x
- Dramatic decrease in \dot{M}_{in} at $L_x/L_{\text{Edd}} > 0.01$ --- transition from net inflow to net outflow



net outflow; non-spherical fragmentation observed.

Thermal instability due to rad. feedback

Non-spherical outflow:

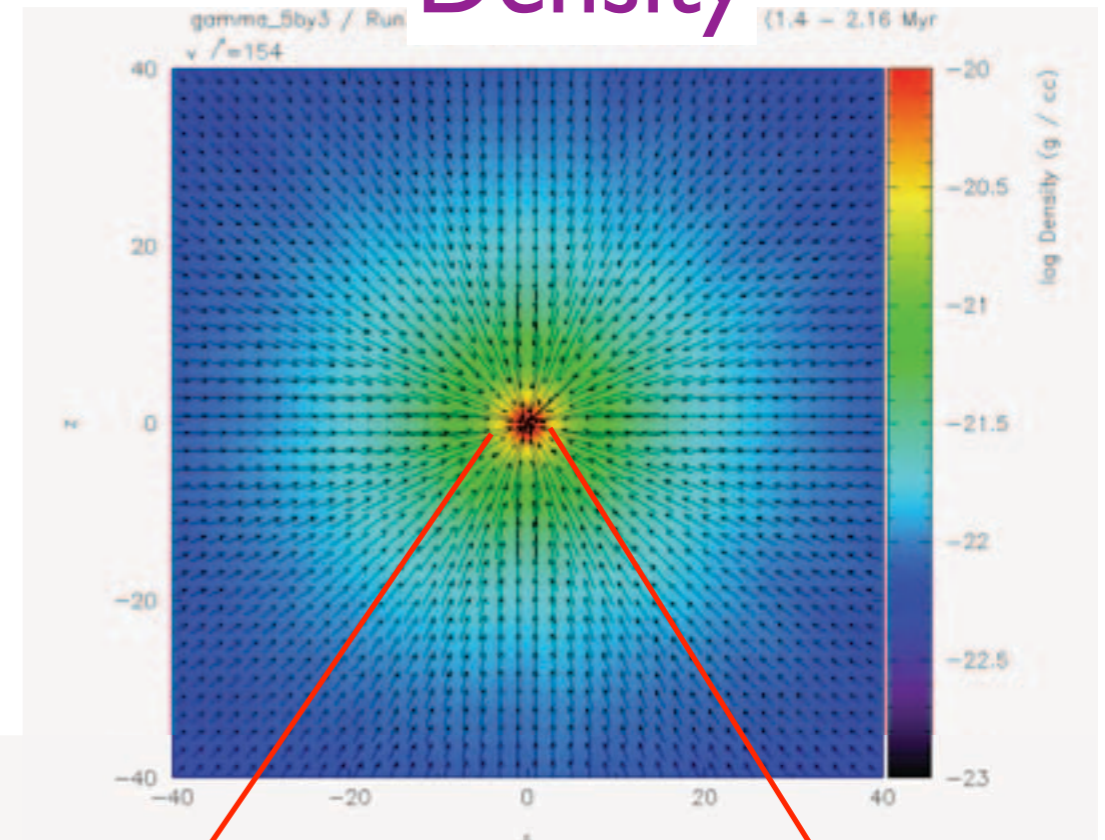
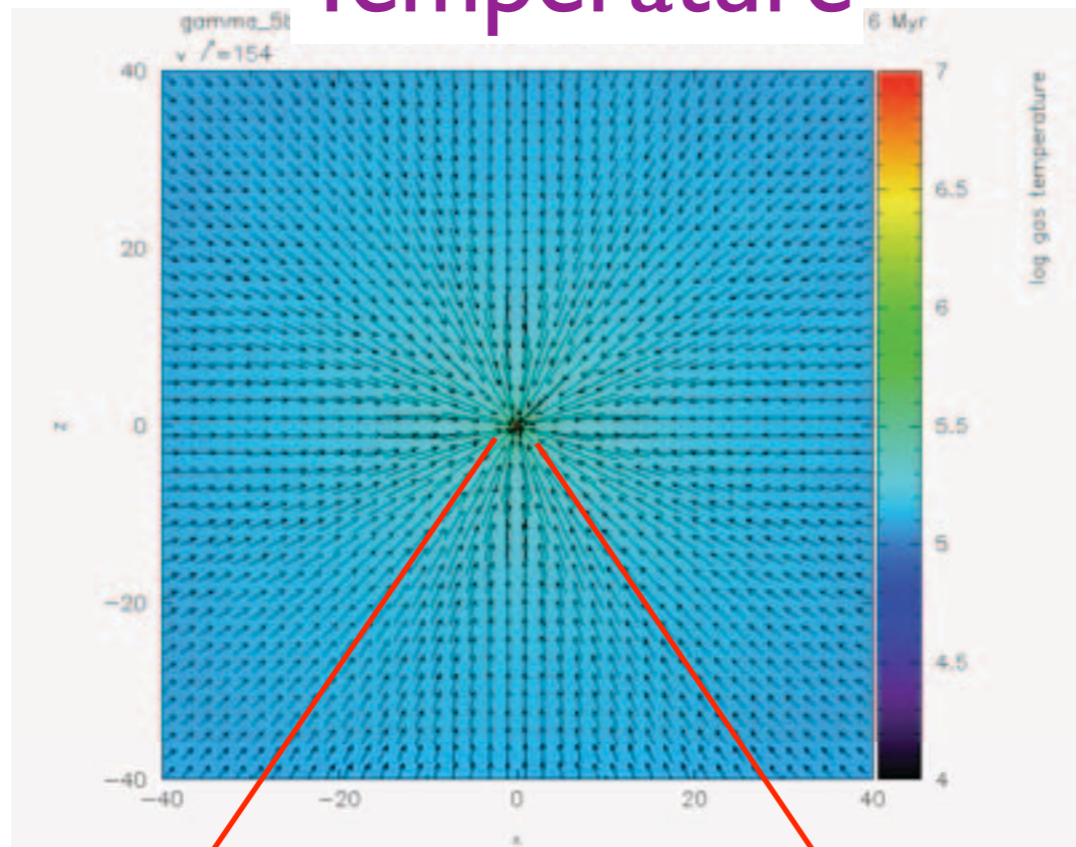
due to rad. feedback

Run 26: $r_{\text{out}}=200\text{pc}$, $L_x/L_{\text{Edd}}=0.01$

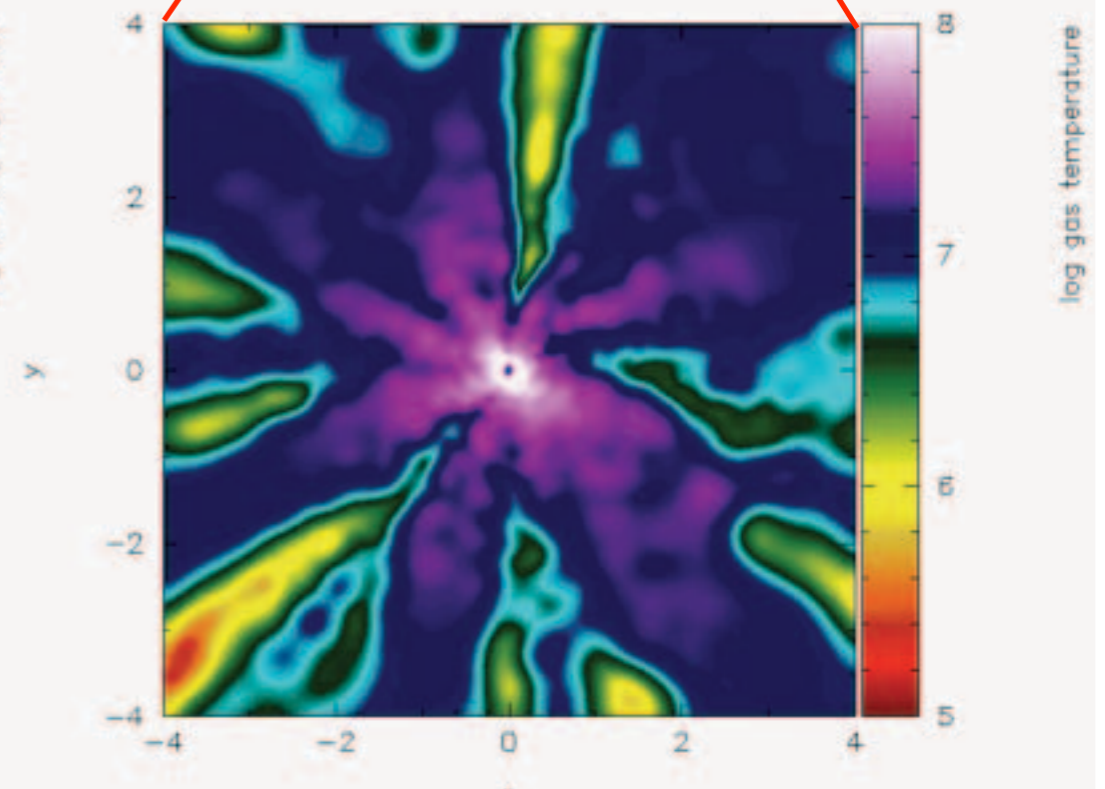
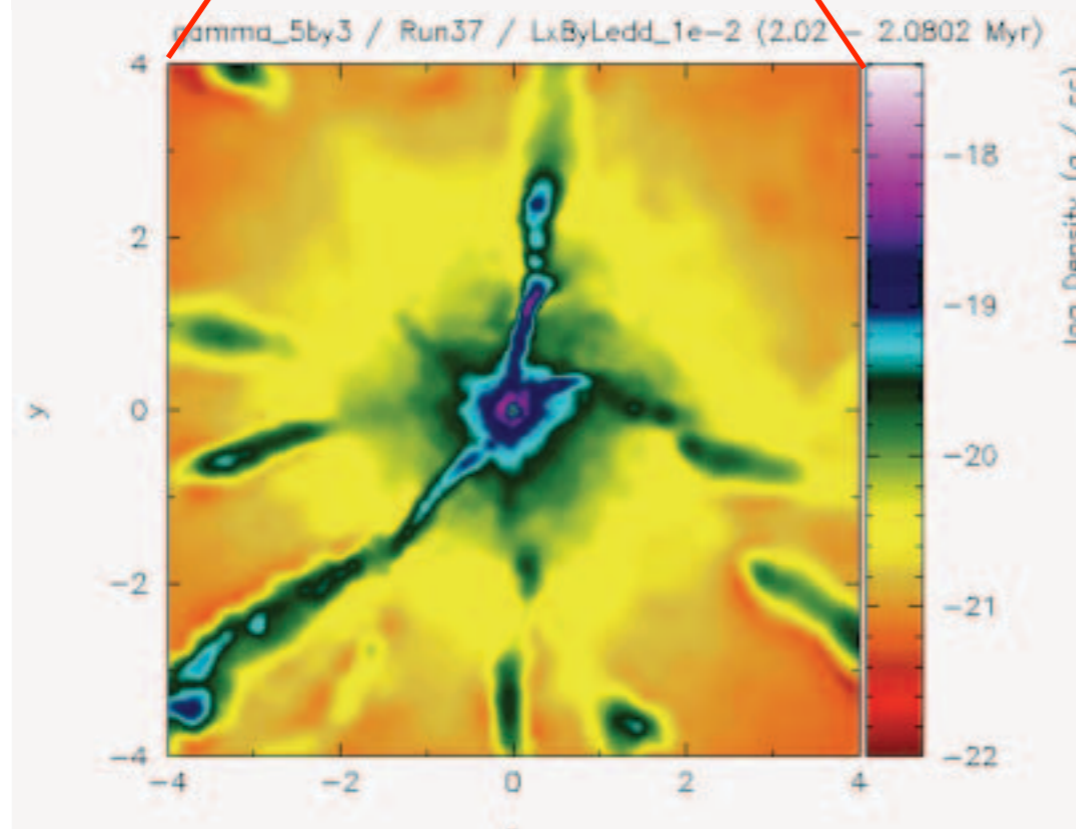
Temperature

Density

inner
 $\pm 40\text{pc}$



inner
 $\pm 4\text{pc}$



Ptcl Properties: impact of rad feedback

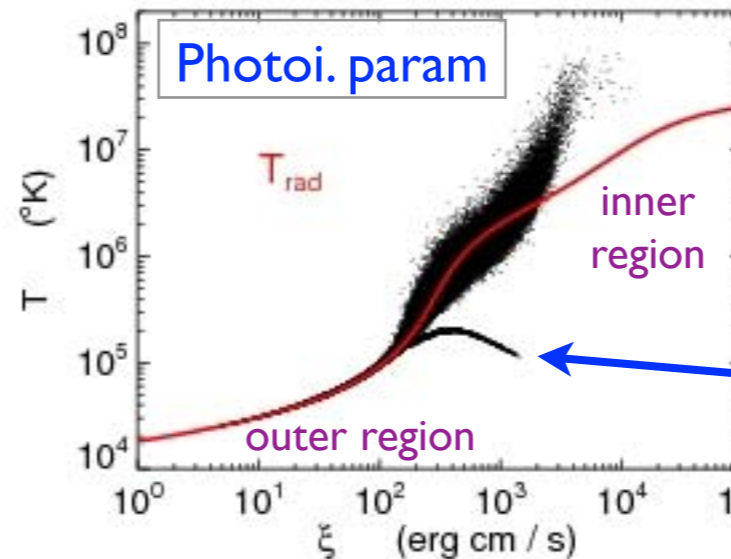
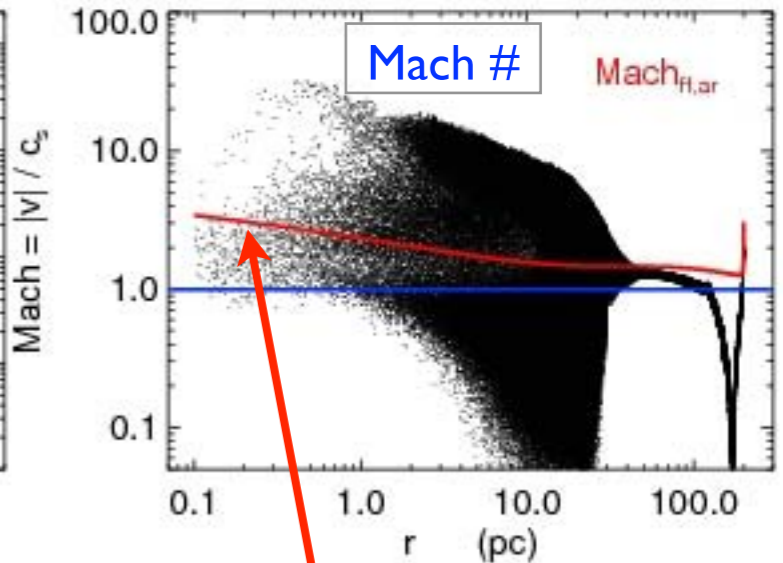
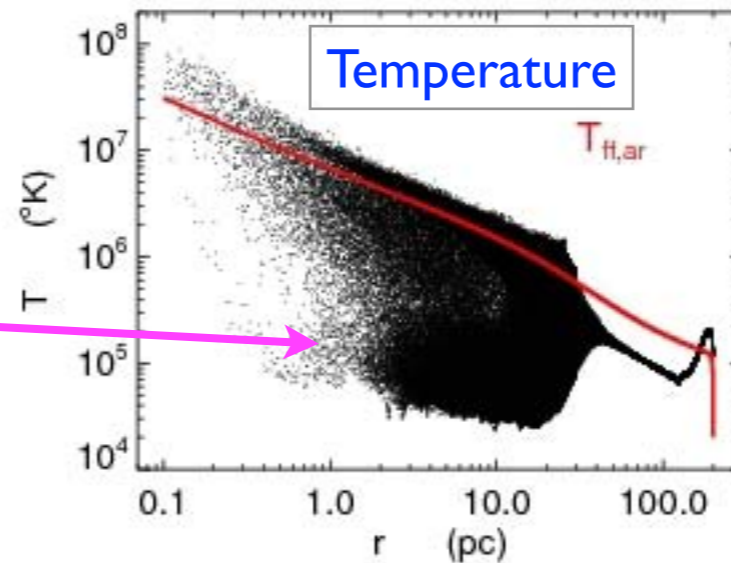
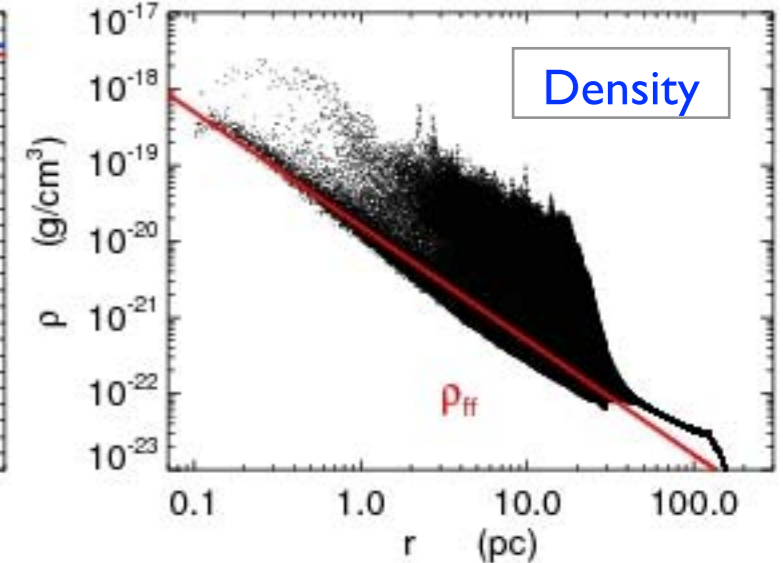
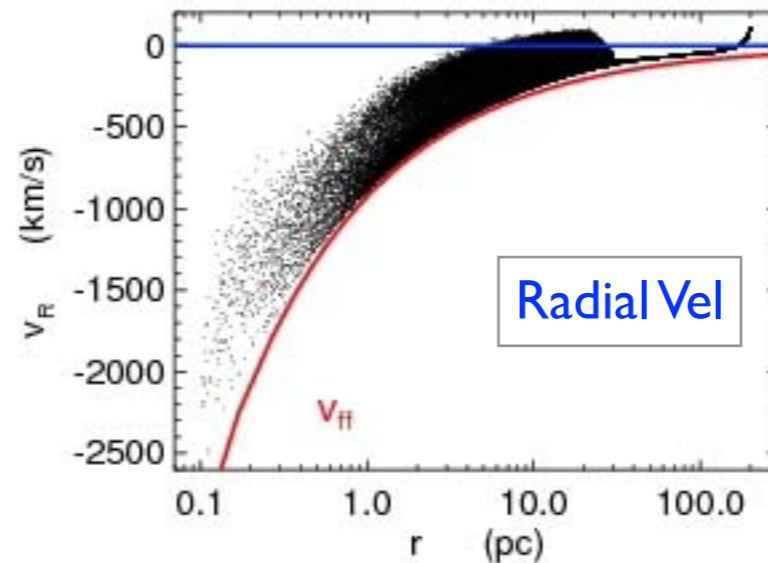
Run 26: $r_{\text{out}}=200\text{pc}$,
 $L_X/L_{\text{Edd}}=0.01$, $t=2.0$
 Myr

Large scatter due to
 thermal instability ---
 cold inflow and hot
 outflow

Cold component

Photoionization parameter:

$$\xi \equiv \frac{4\pi F_X}{n} = \frac{L_X}{r^2 n}$$



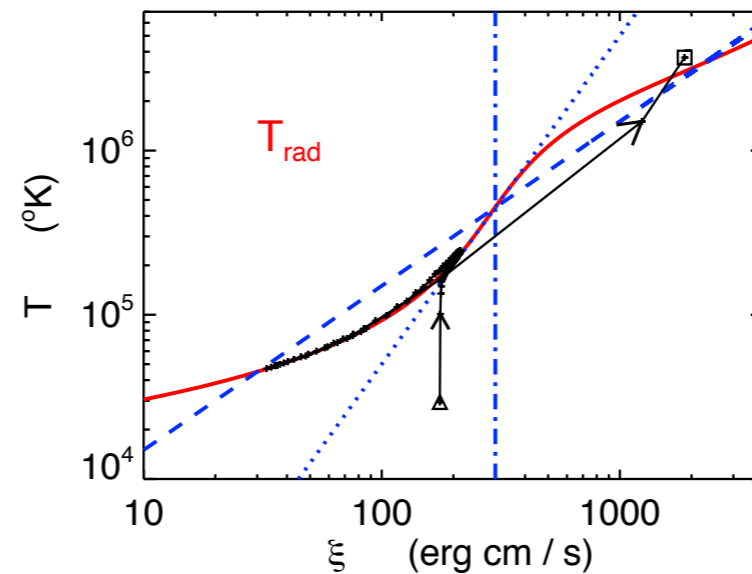
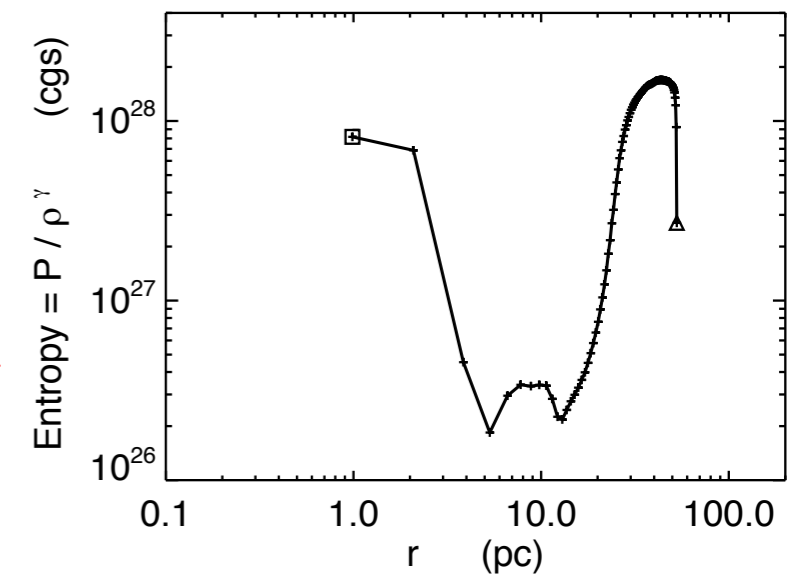
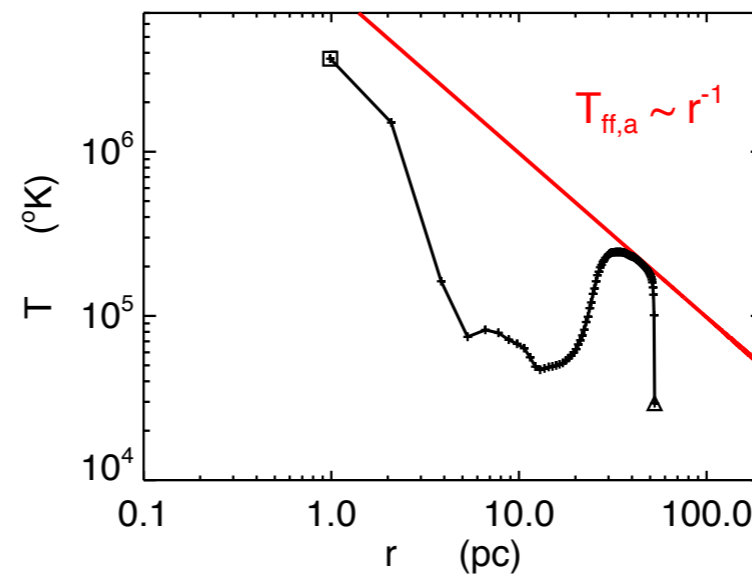
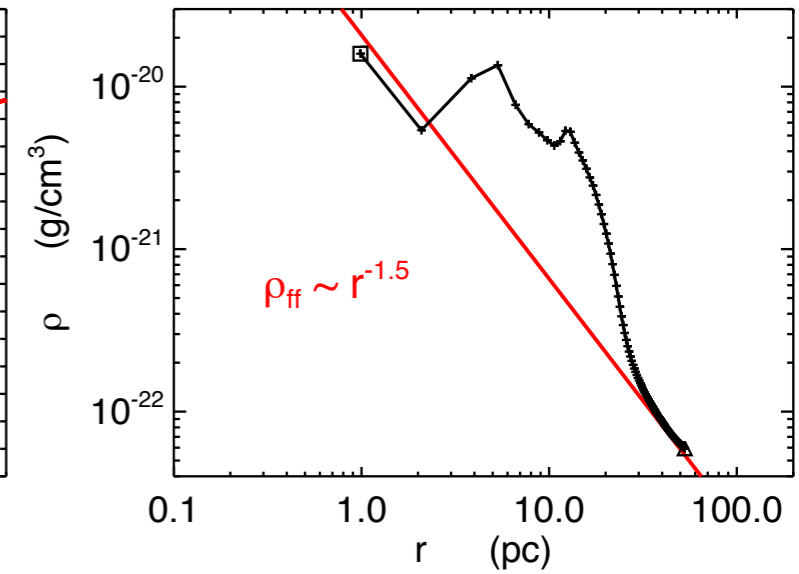
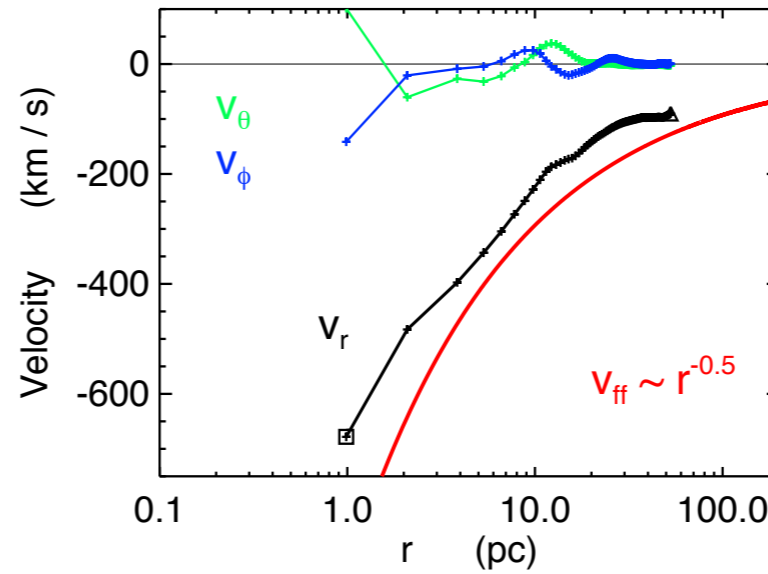
Radiative equil.

Outflowing gas
 near outer BC

Time Evolution of a Single Ptcl

Run 26: $r_{\text{out}}=200\text{pc}$,
 $L_x/L_{\text{Edd}}=0.01$, $t=2.0$
 Myr

- Start (triangle): $r=53\text{ pc}$,
 $t=1.4\text{ Myr}$
- End (square): $r=1\text{ pc}$, $t=1.8$
 Myr
- + symbol: $dt=0.004\text{ Myr}$



Non-spherical outflow:

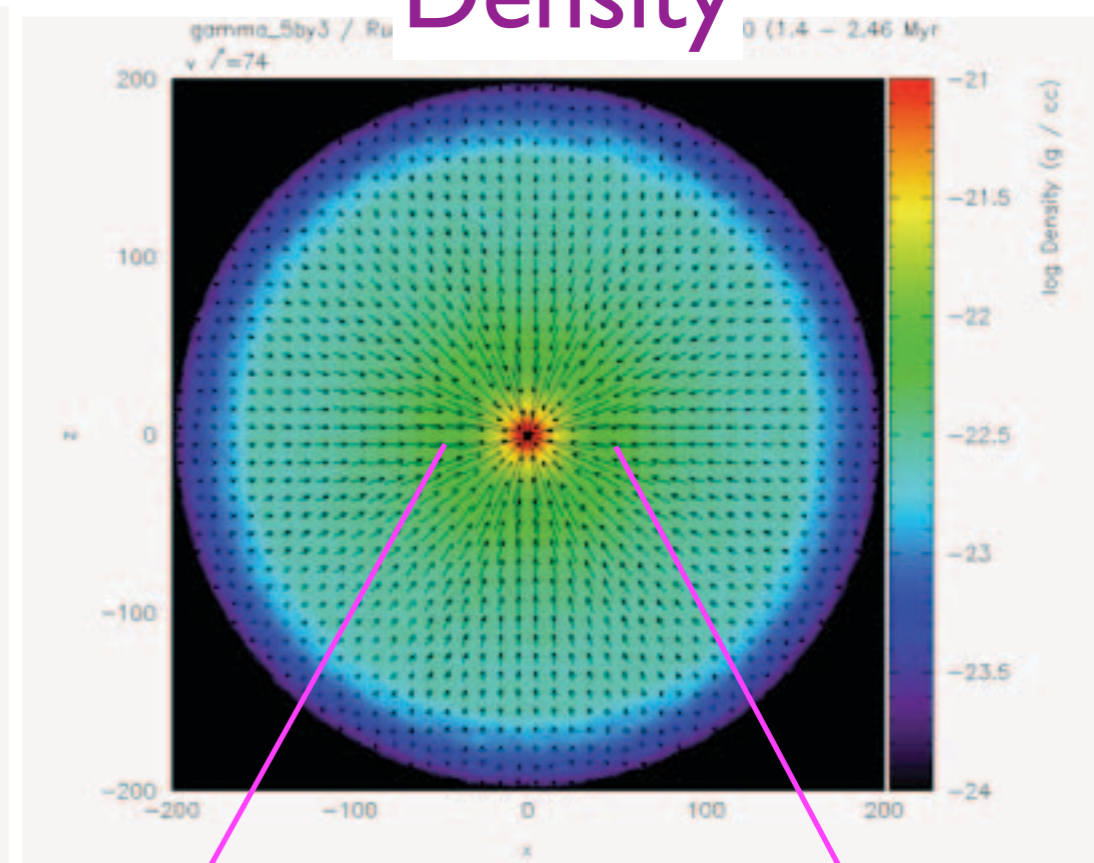
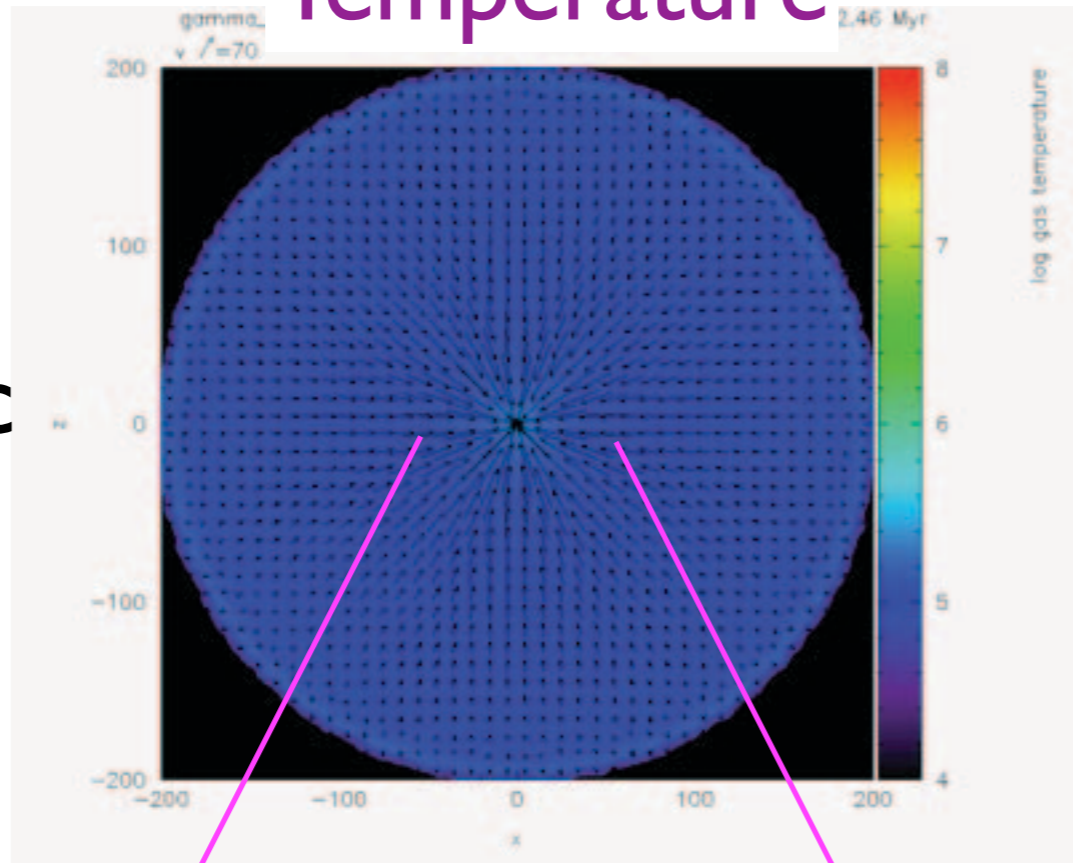
due to rad. feedback

Run 27: $r_{\text{out}}=200\text{pc}$, $L_x/L_{\text{Edd}}=0.02$

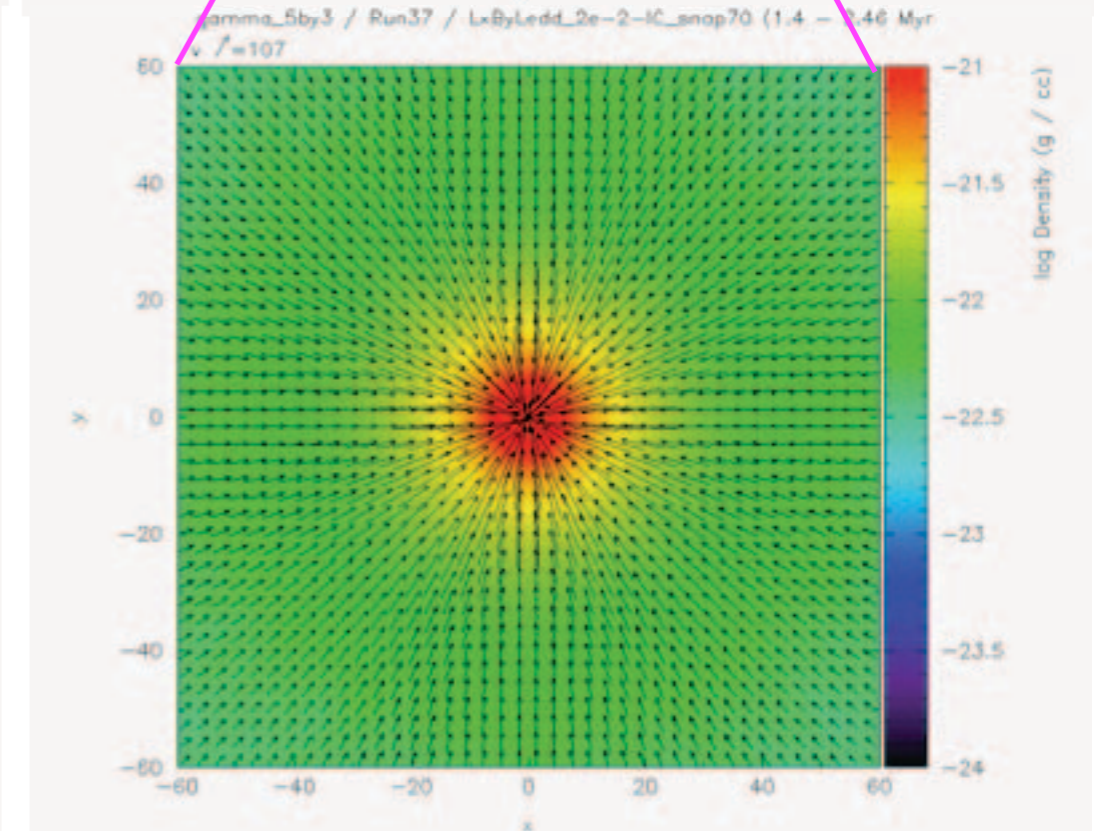
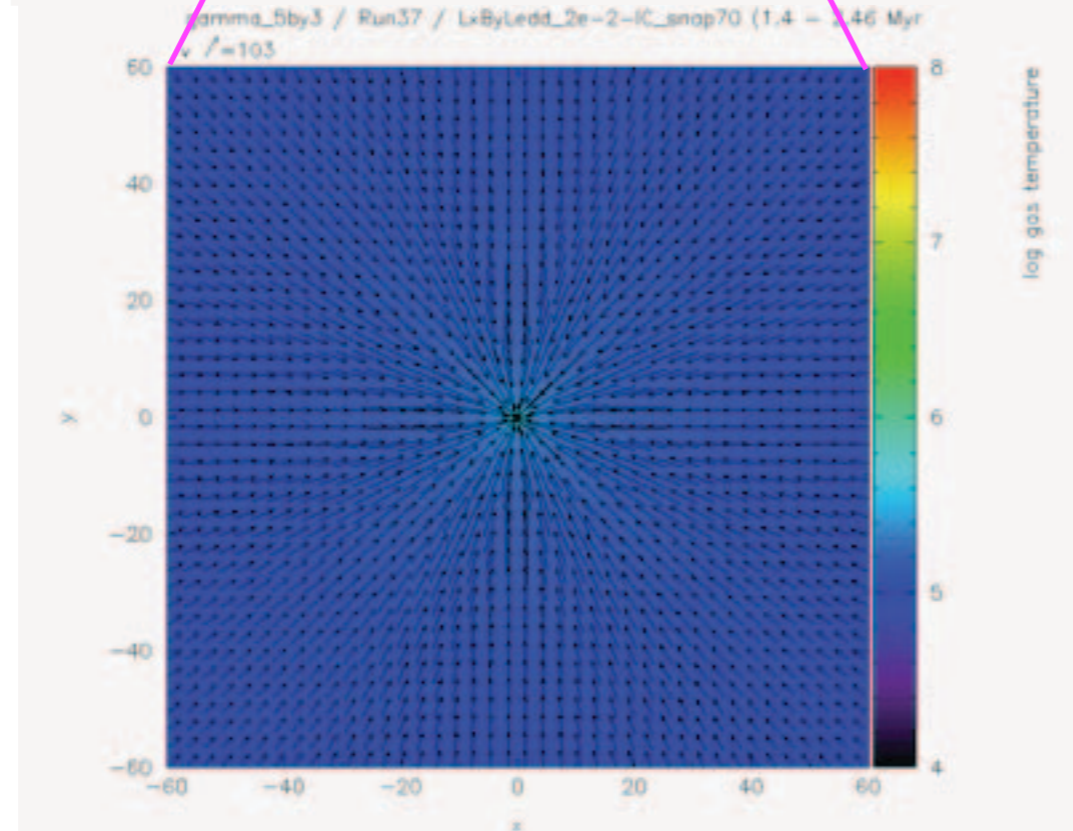
Temperature

Density

$\pm 200\text{pc}$

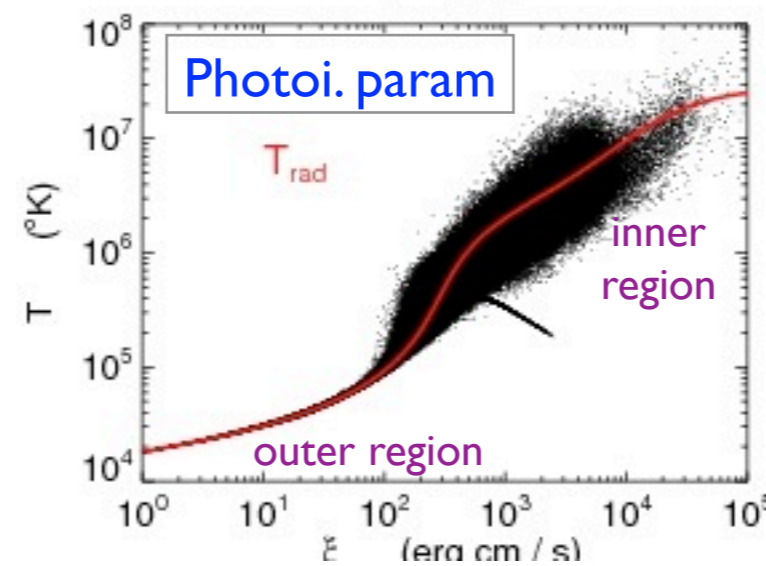
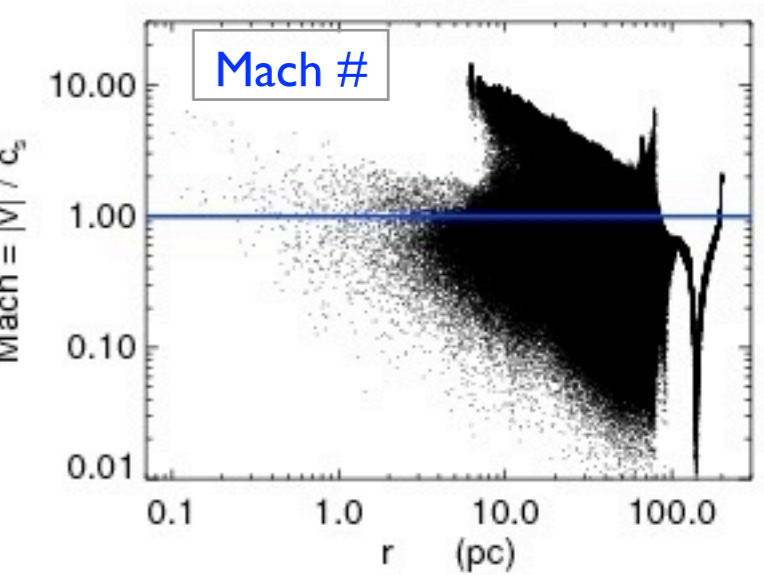
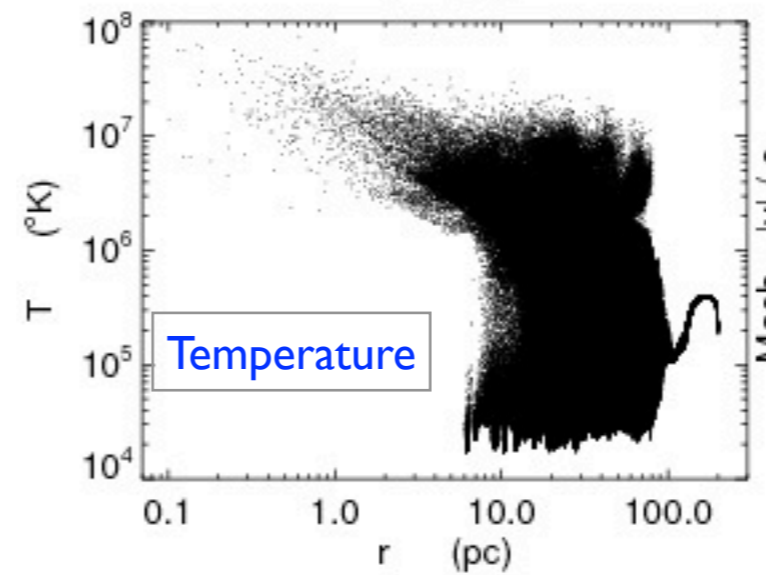
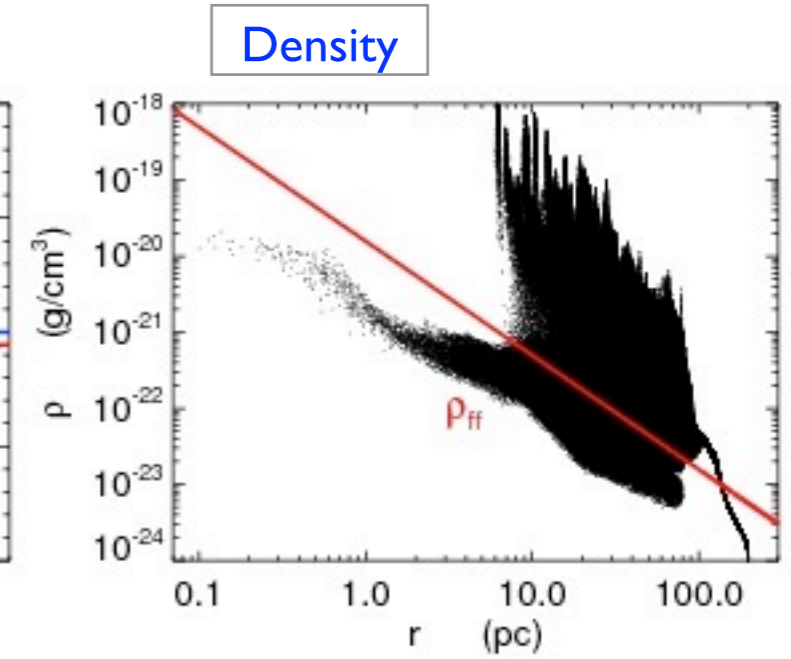
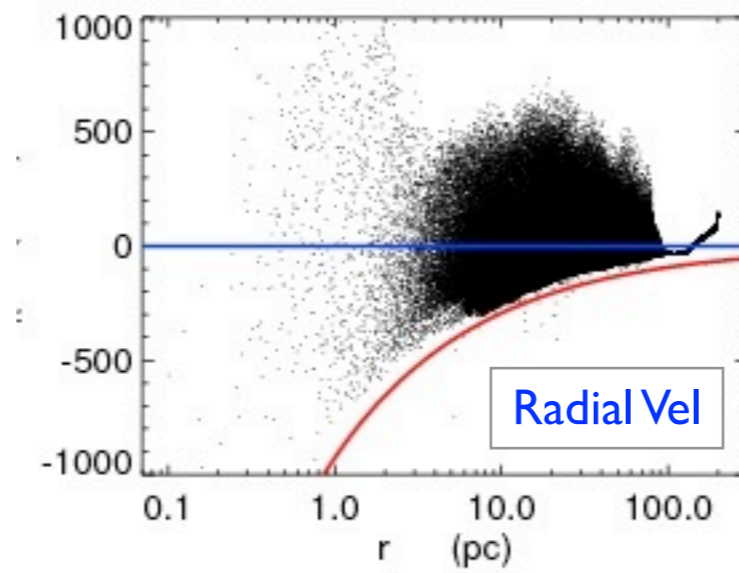


inner
 $\pm 60\text{pc}$



Ptcl Properties: impact of rad feedback

Run 27: $r_{\text{out}}=200\text{pc}$,
 $L_x/L_{\text{Edd}}=0.02$

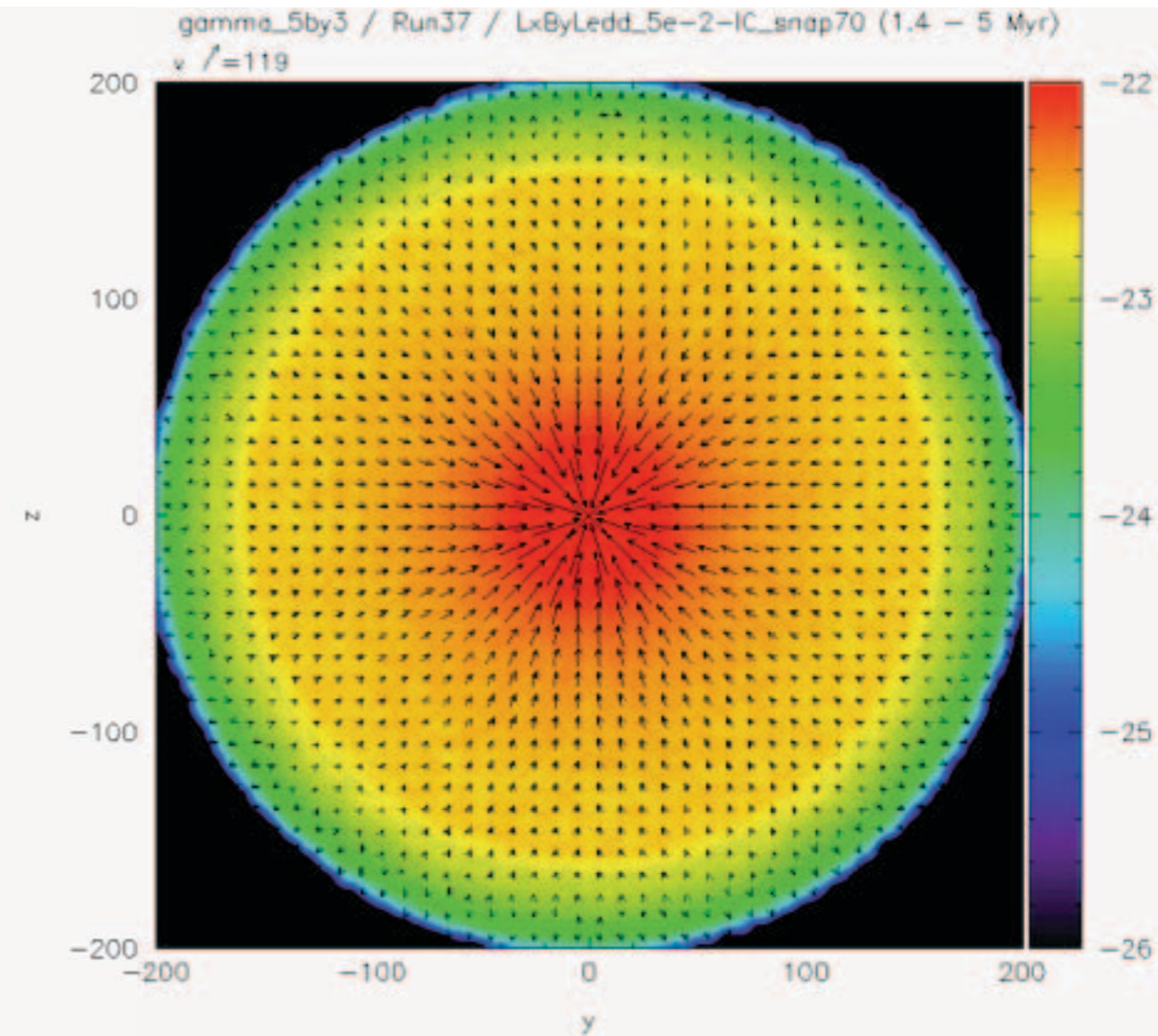
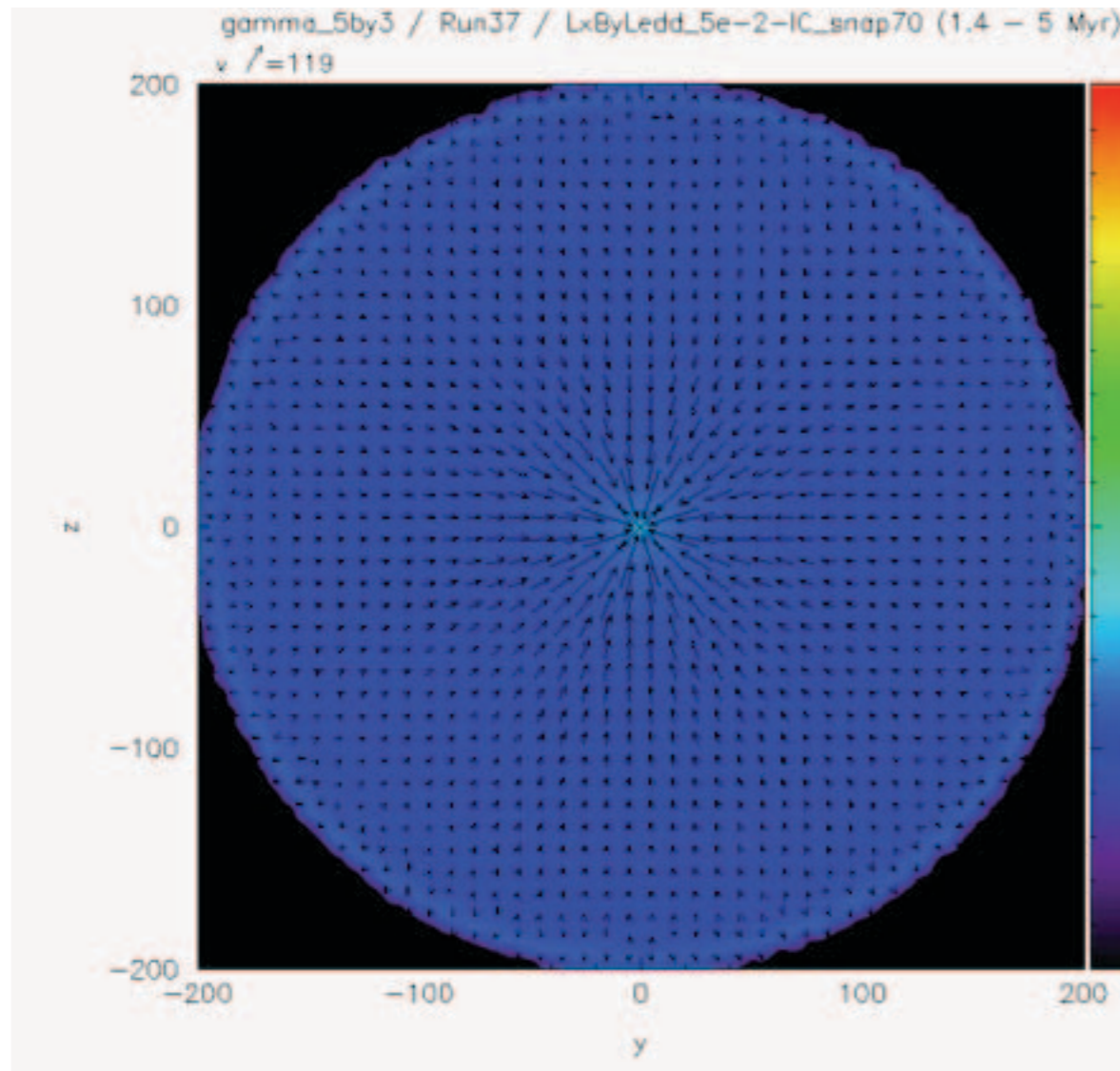


Non-spherical outflow: due to rad. feedback

Run 28: $r_{\text{out}}=200\text{pc}$, $L_x/L_{\text{Edd}}=0.05$

Temperature

Density

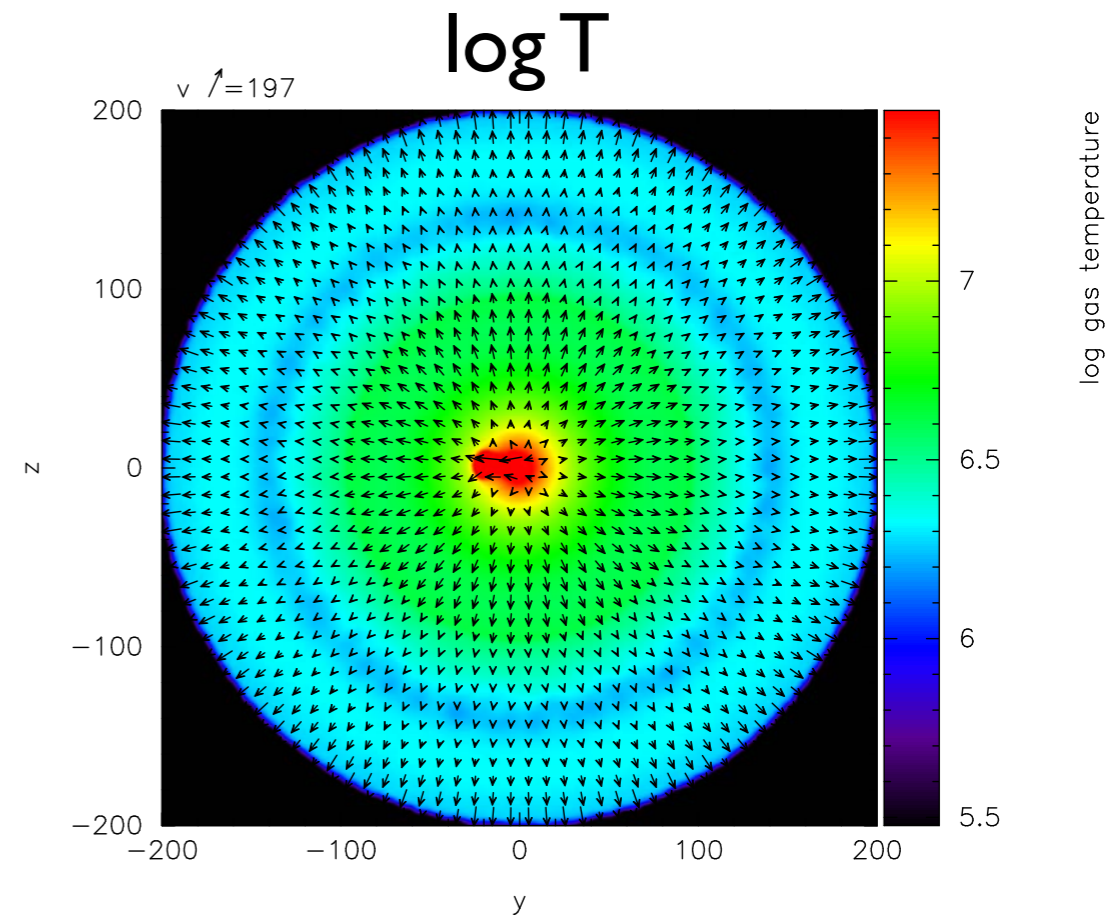
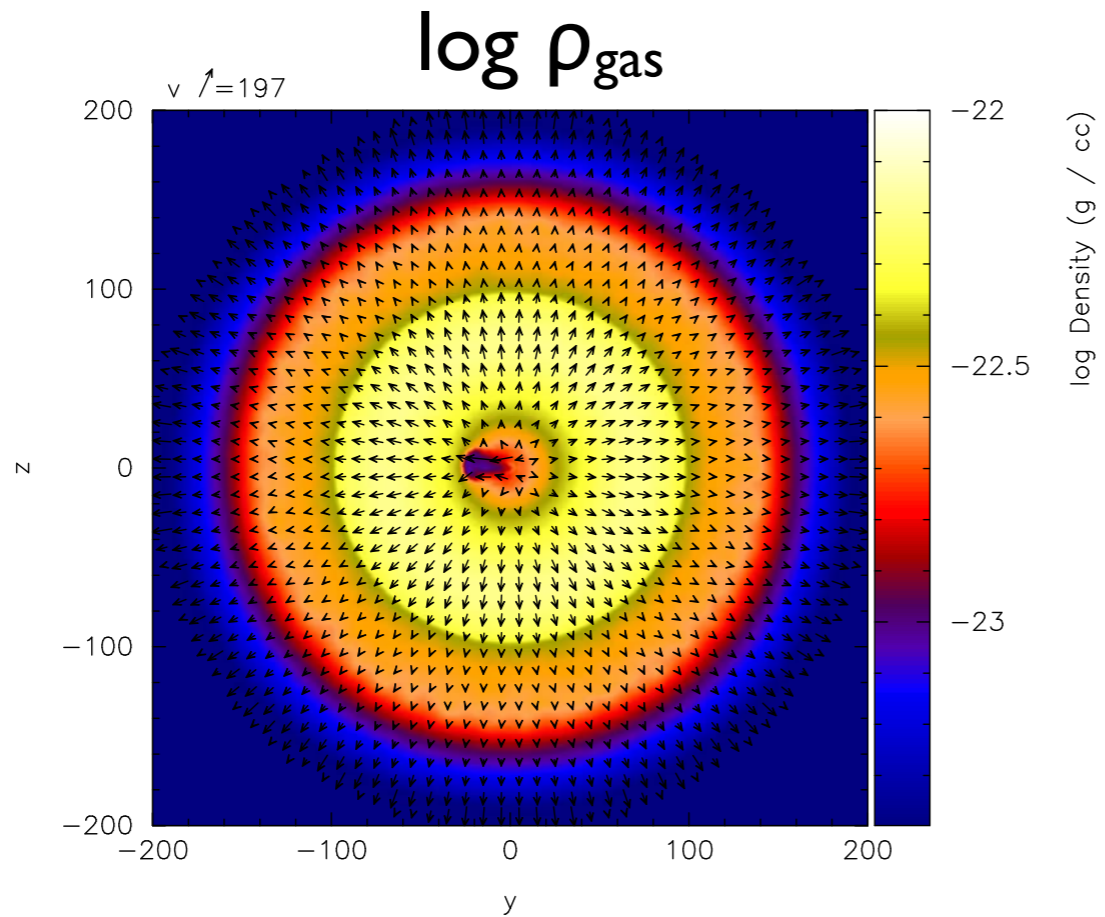


$\pm 200\text{pc}$

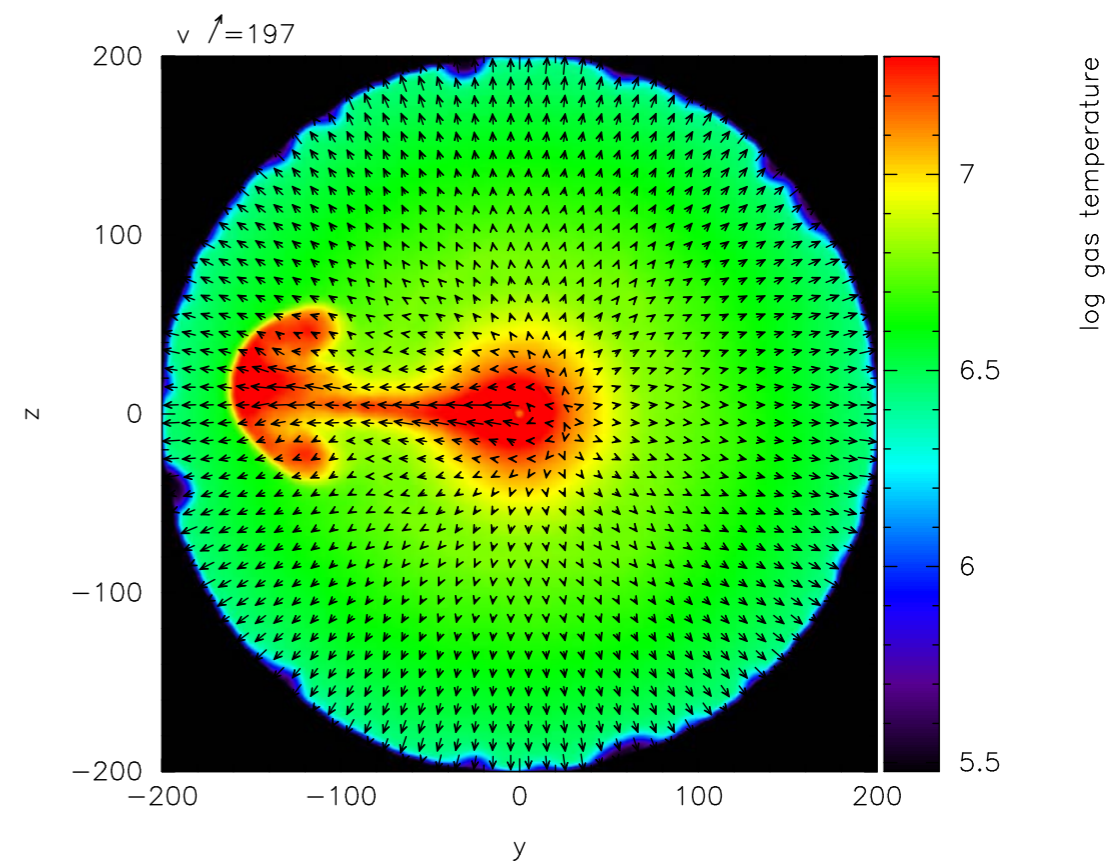
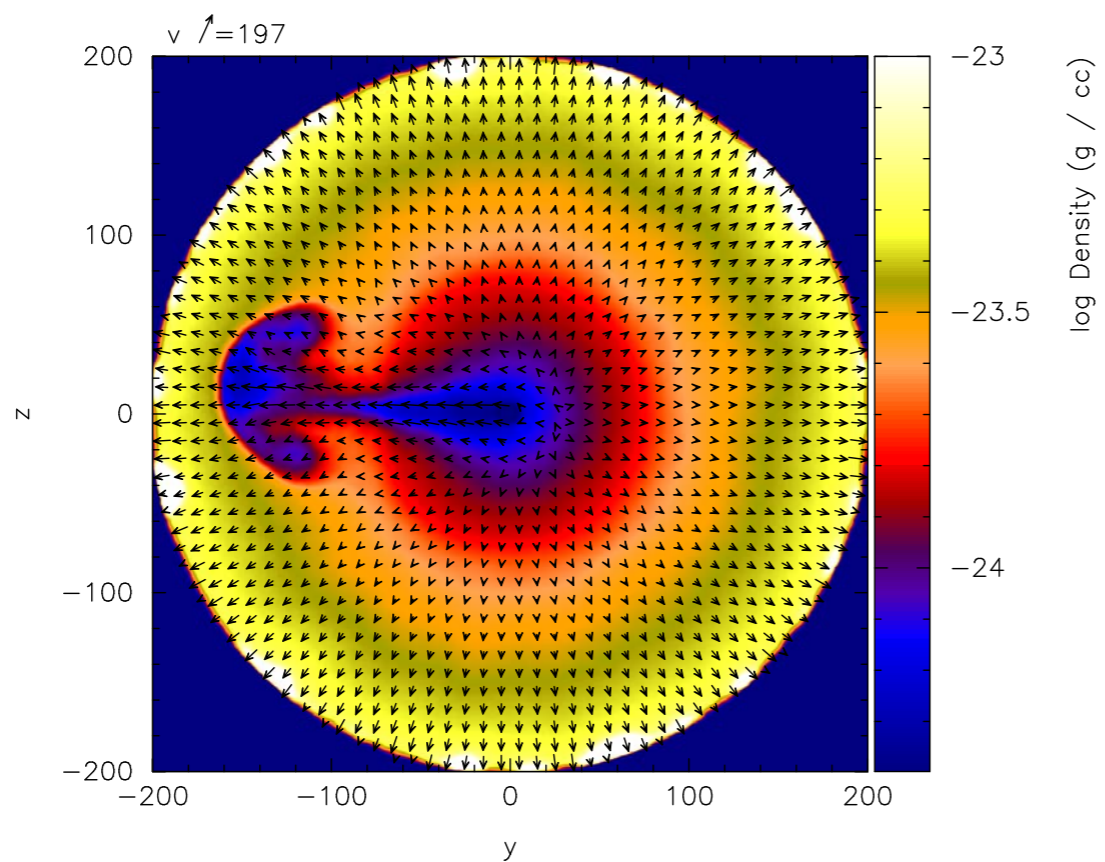
Run 28

$r_{\text{out}}=200\text{pc}, L_x/L_{\text{Edd}}=0.05$

$t=1.8\text{ Myr}$



$t=3.0\text{ Myr}$

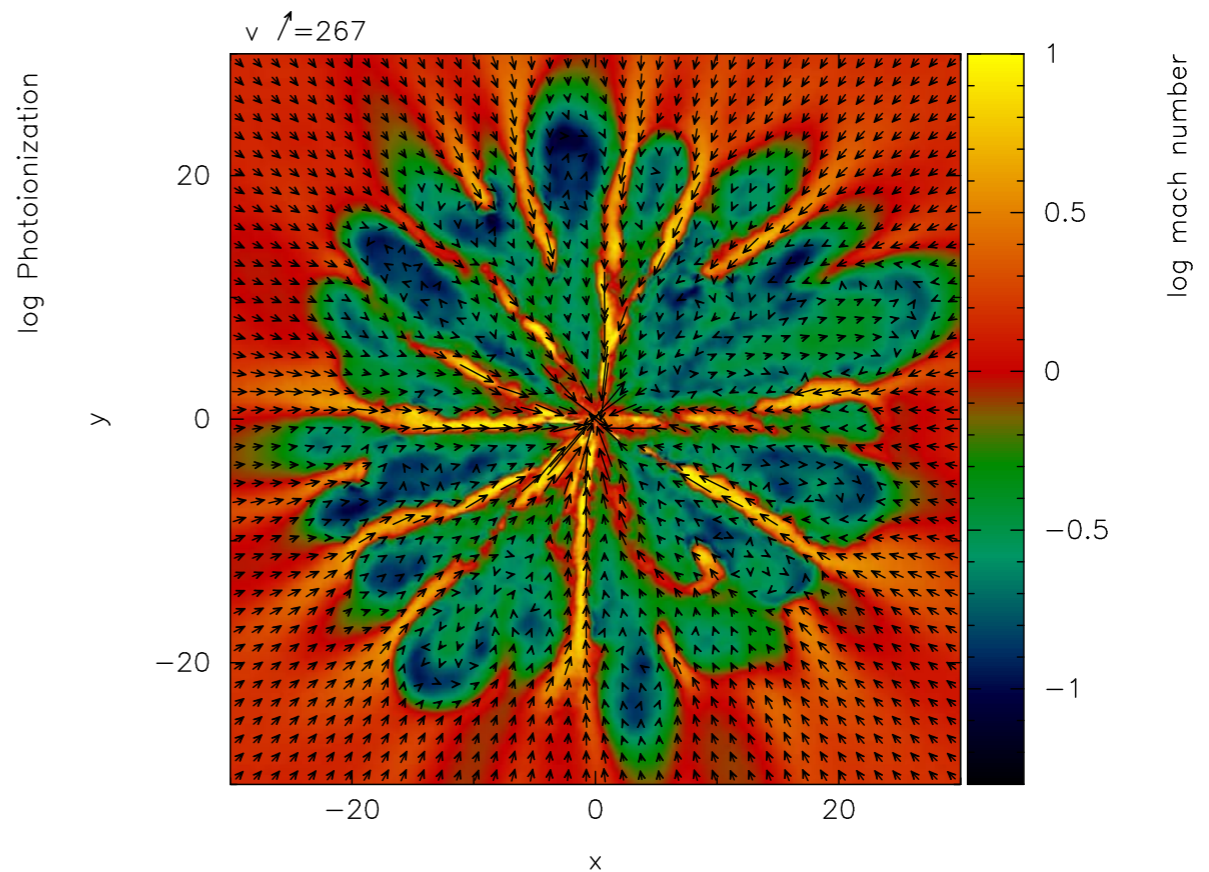
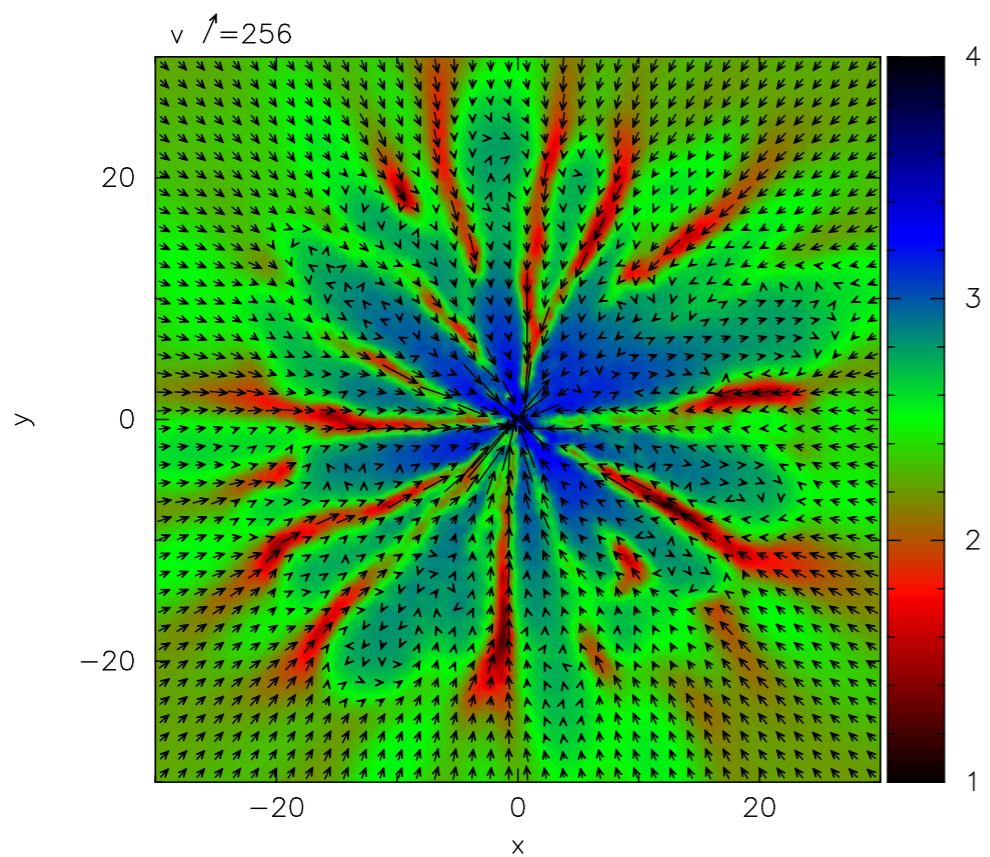
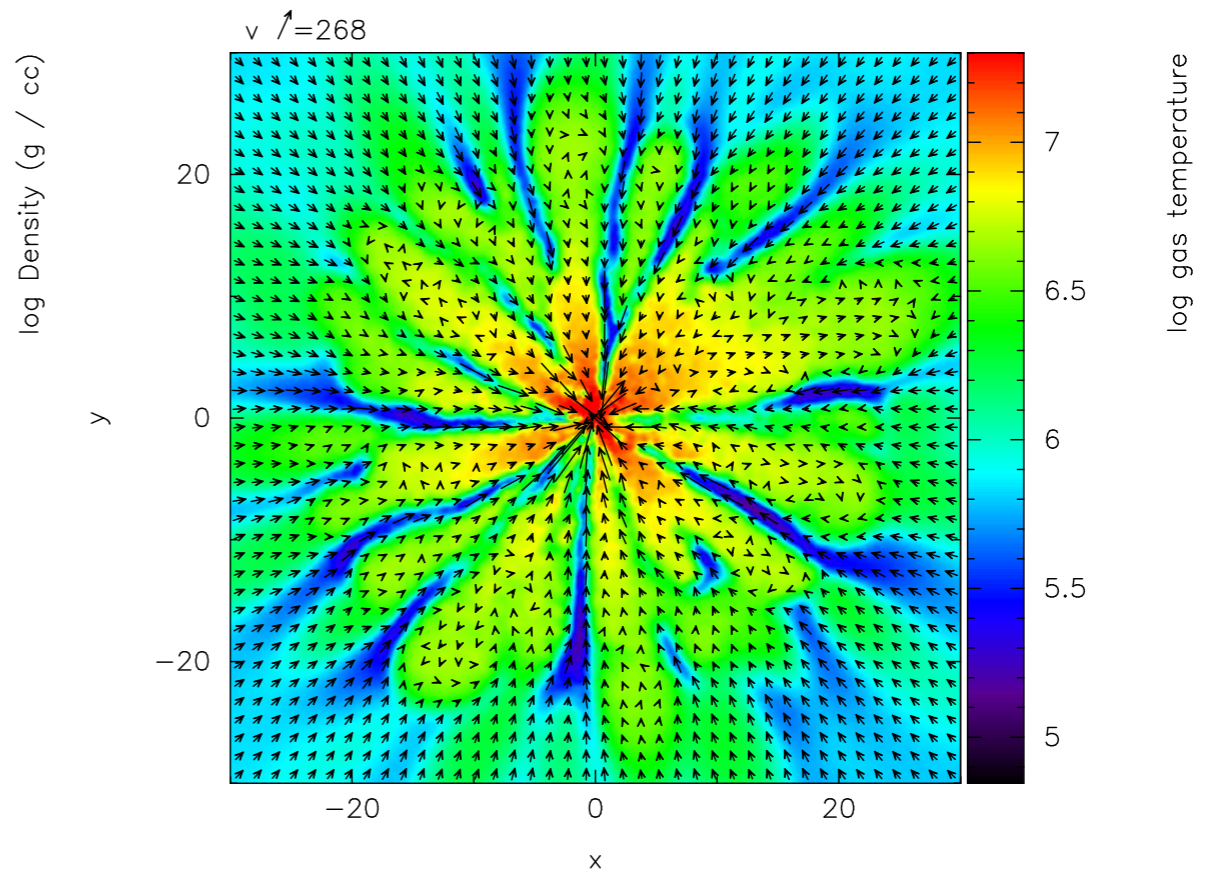
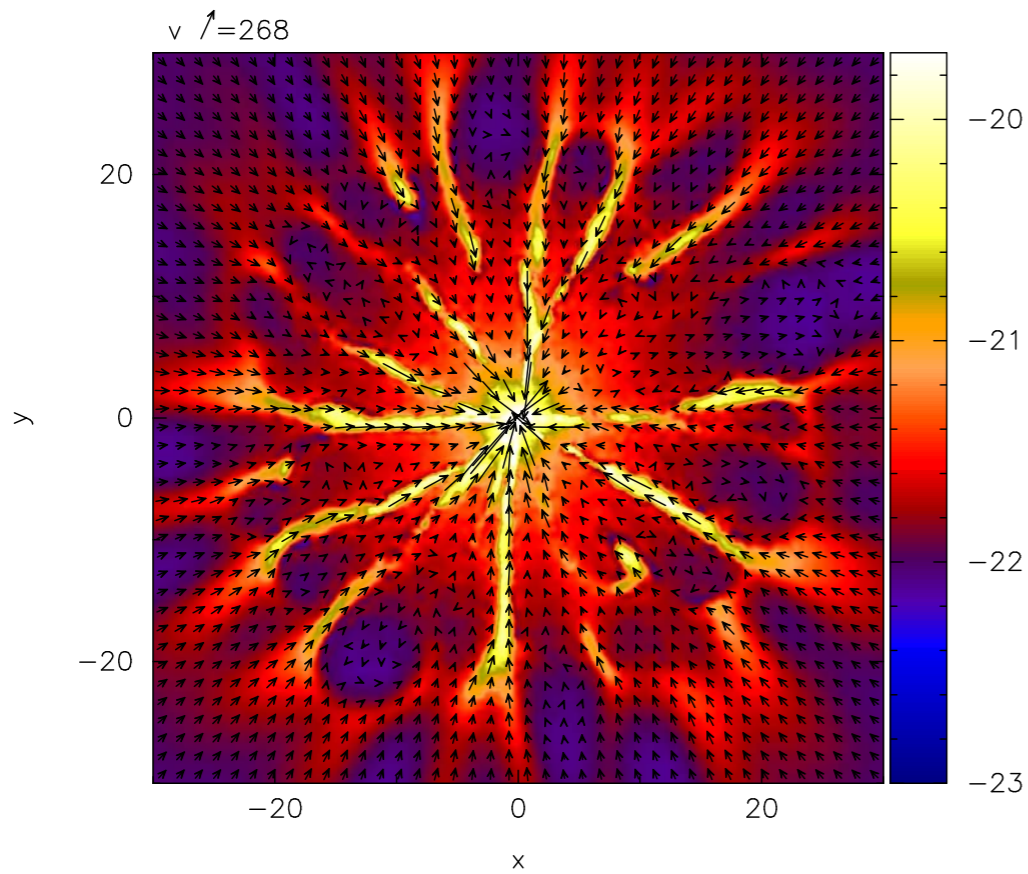


Conclusions

- GADGET-3 SPH code can reproduce the spherical Bondi accretion rate properly, but with some limitations.
- spurious heating by **Artificial Viscosity** near r_{in} & artificial outflow at r_{out} due to outer BC are problems for SPH.
- **non-spherical in/outflow** develops due to **rad. feedback** via **thermal instability**, even in the simplest situation that we studied --- connection with NLR? (Paper II)
- Future work: include rad. pressure, rotation, diff geometry, comparison w/ NLR obs, connect with cosmological sim

Run 26: $r_{\text{out}}=200\text{pc}$, $L_x/L_{\text{Edd}}=0.01$

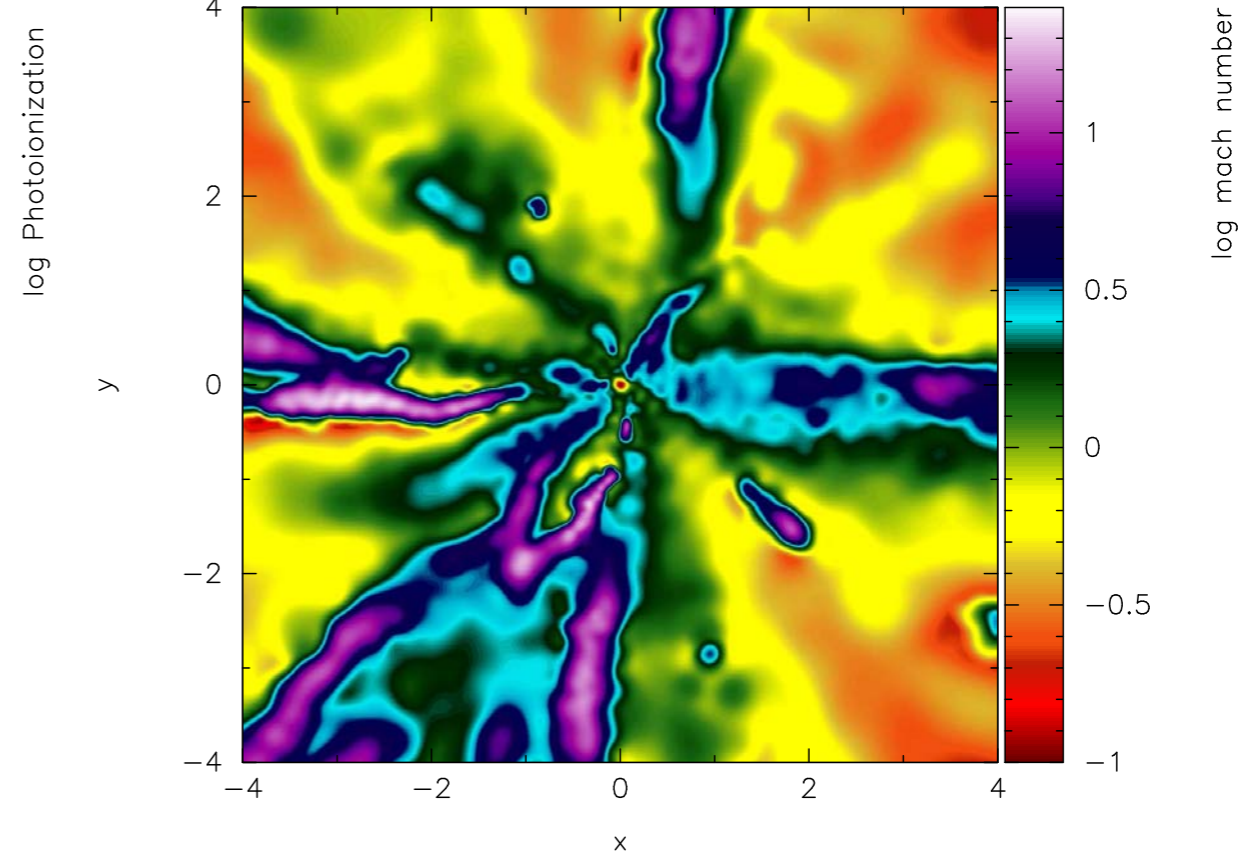
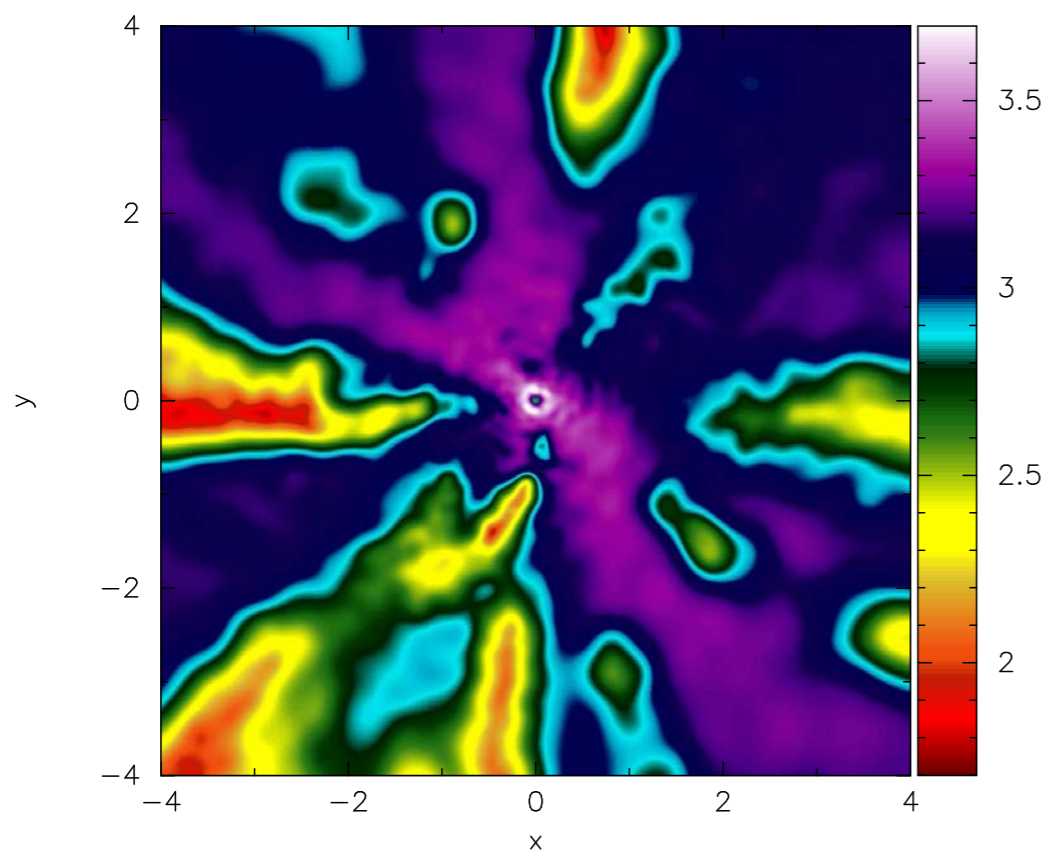
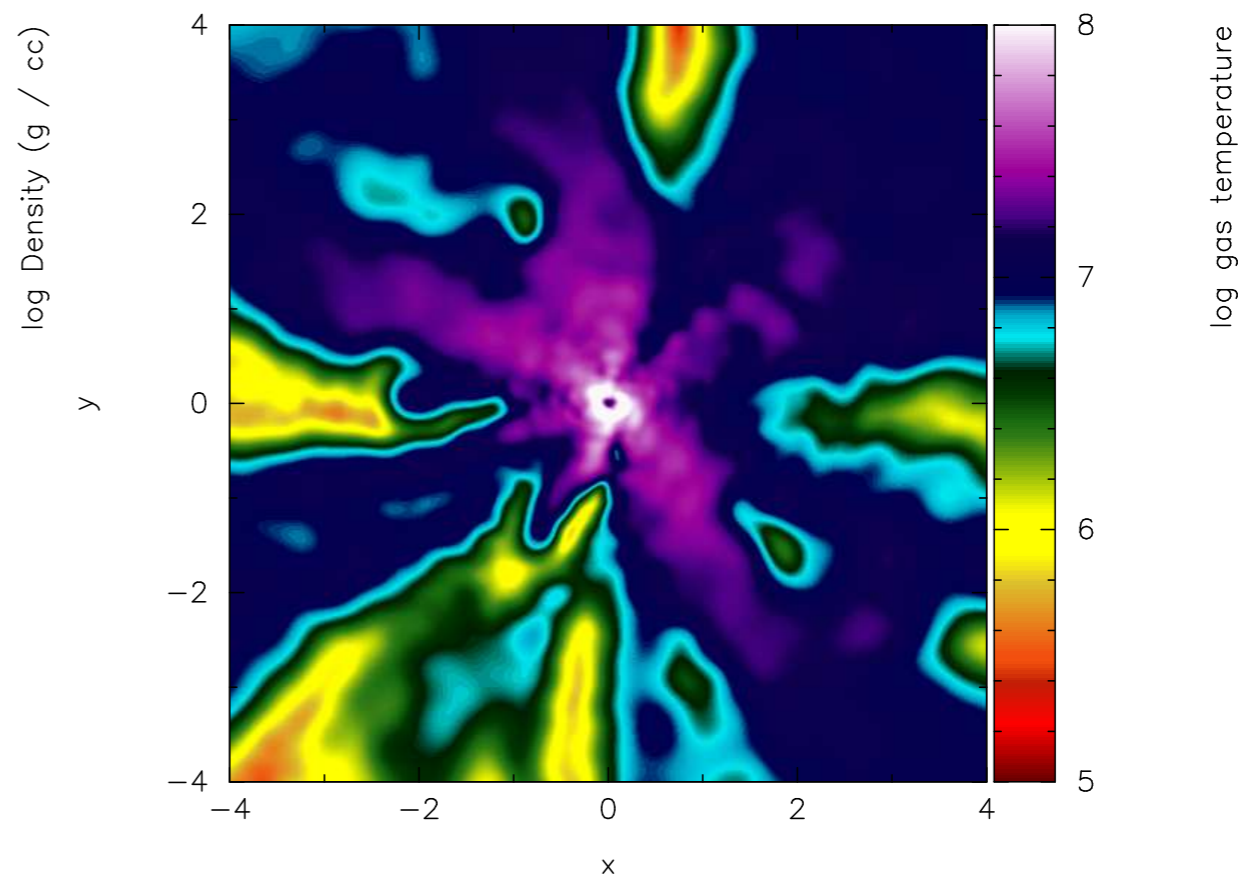
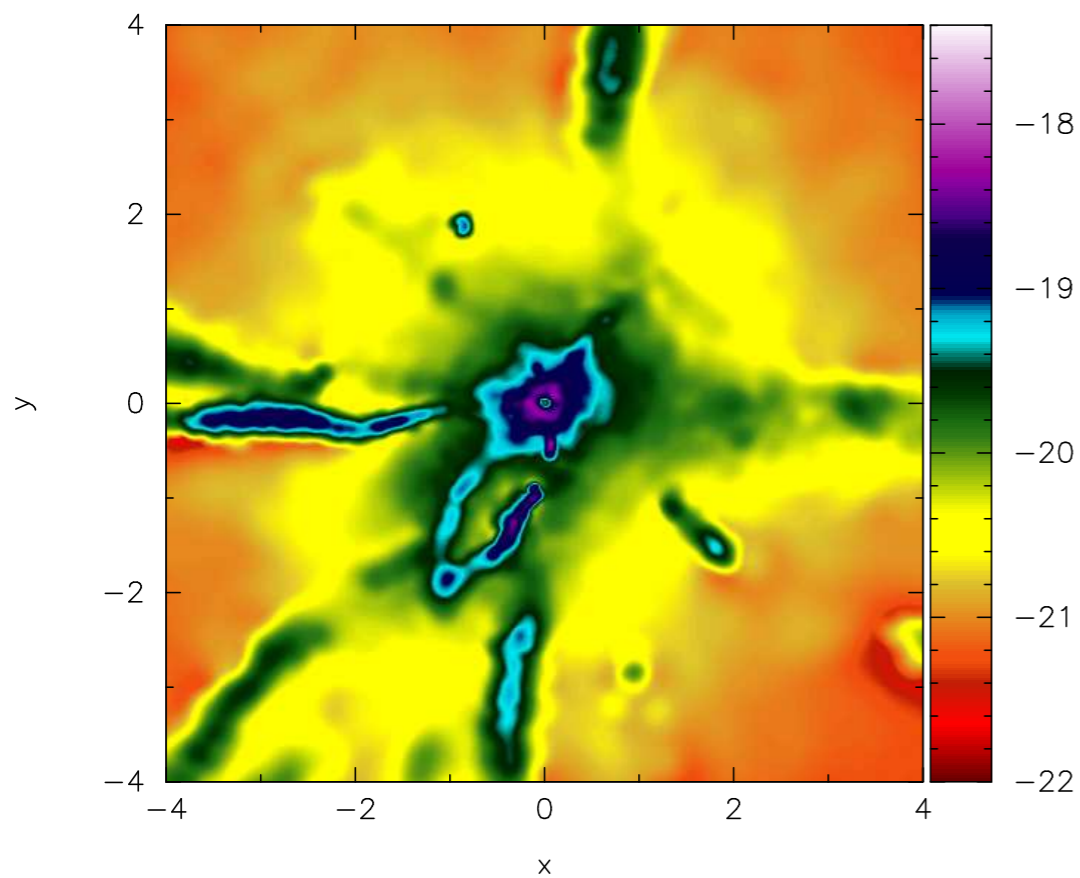
$\pm 30\text{ pc range}$ ($t = 2.047\text{ Myr}$)



colder, denser filament-like structures due to non-spherical fragmentation

Run 26: $r_{\text{out}}=200\text{pc}$, $L_x/L_{\text{Edd}}=0.01$

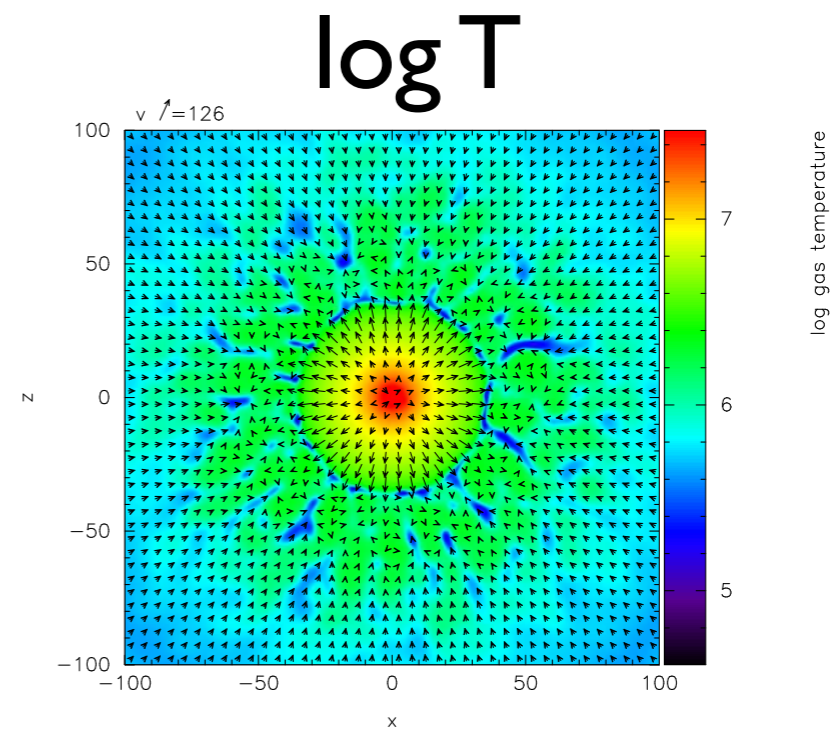
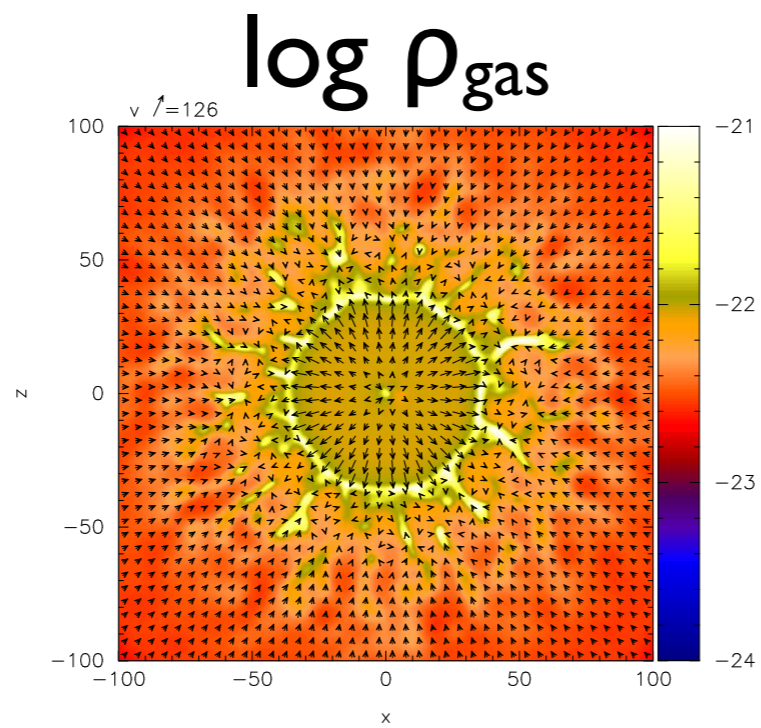
Zoom-in: inner 4 pc



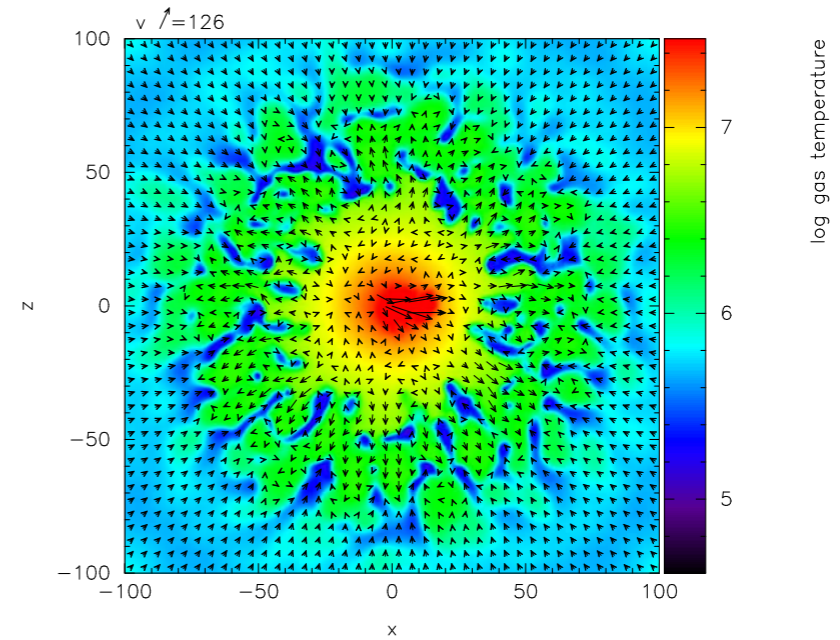
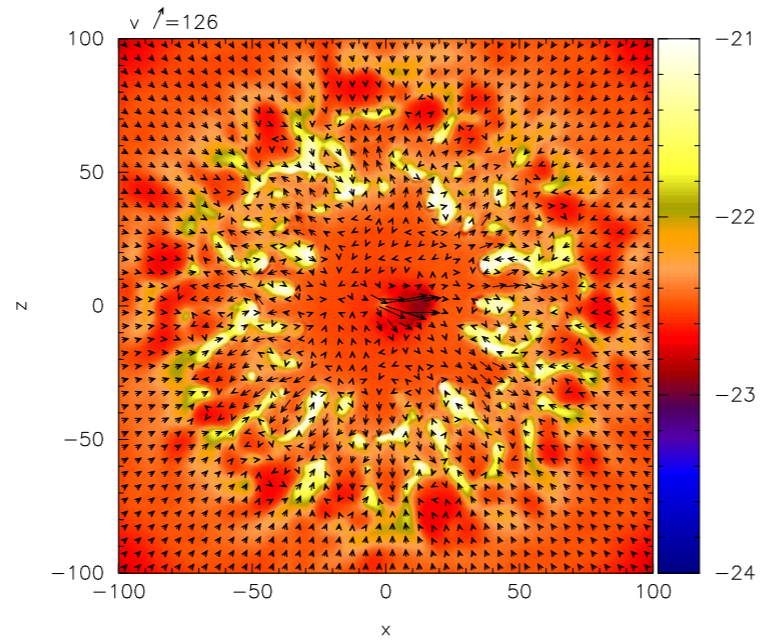
Run 27

$r_{\text{out}}=200\text{pc}$,
 $L_x/L_{\text{Edd}}=0.02$

$t=1.86\text{ Myr}$



$t=2.12\text{ Myr}$



$t=2.46\text{ Myr}$

